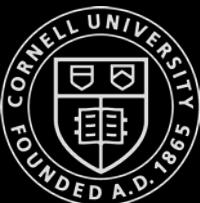


ECE 4960

Prof. Kirstin Hagelskjær Petersen
kirstin@cornell.edu

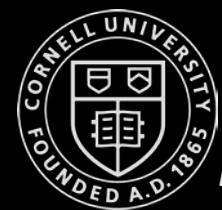
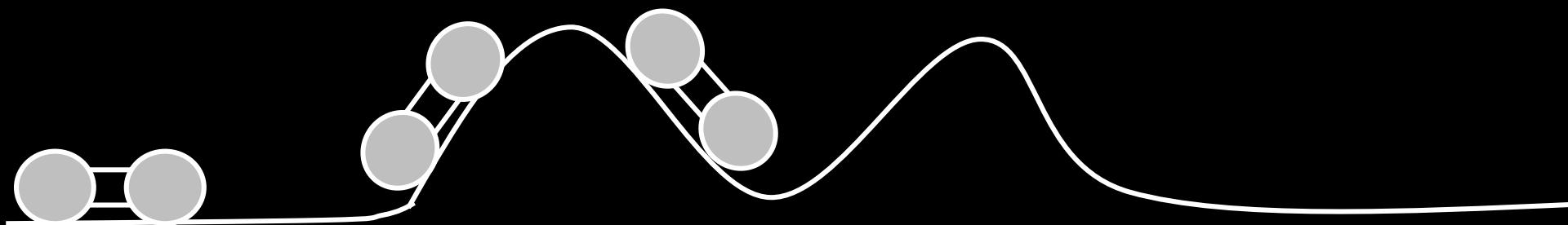
Fast Robots



ECE4960 Fast Robots

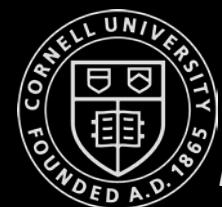
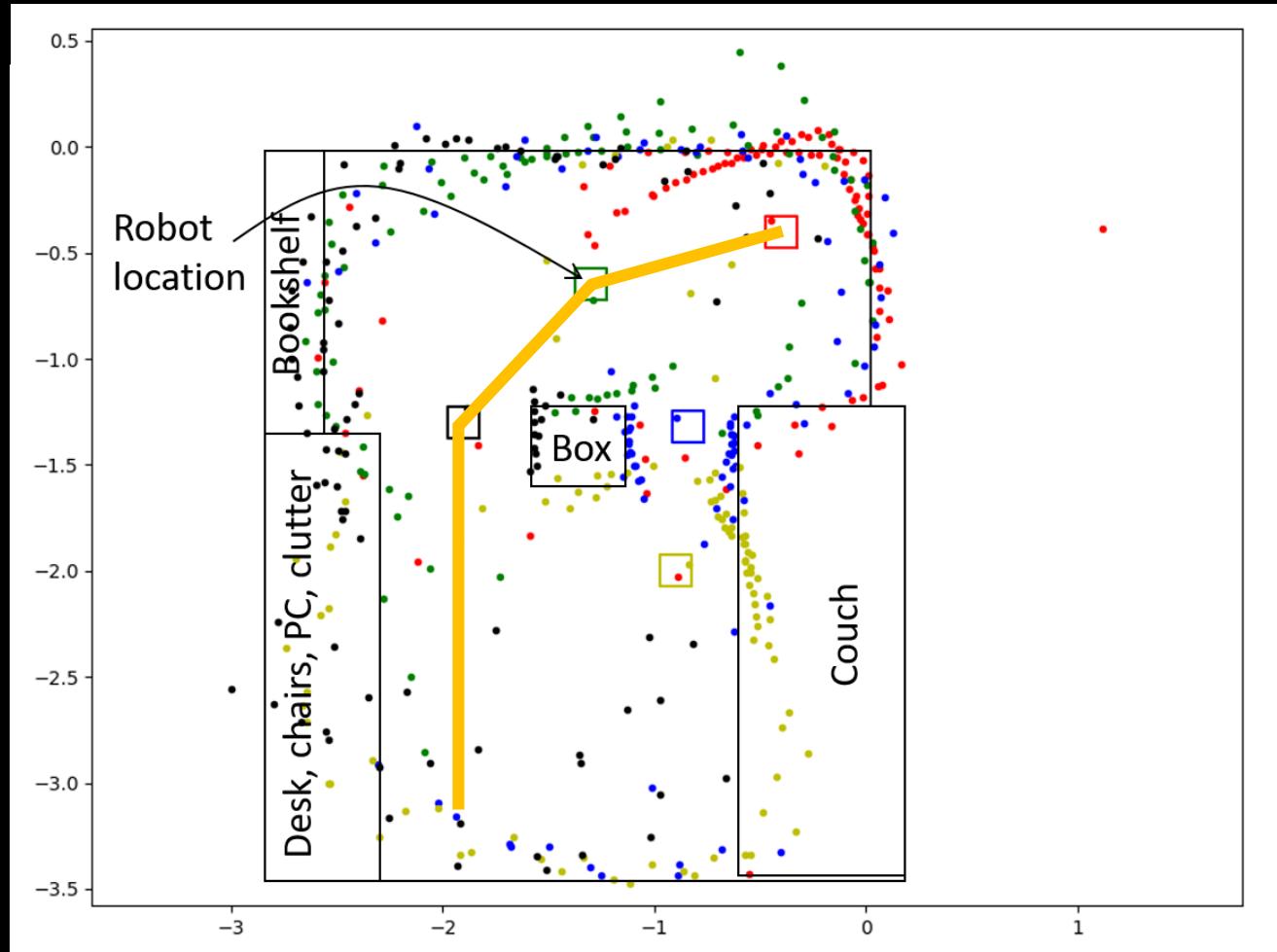
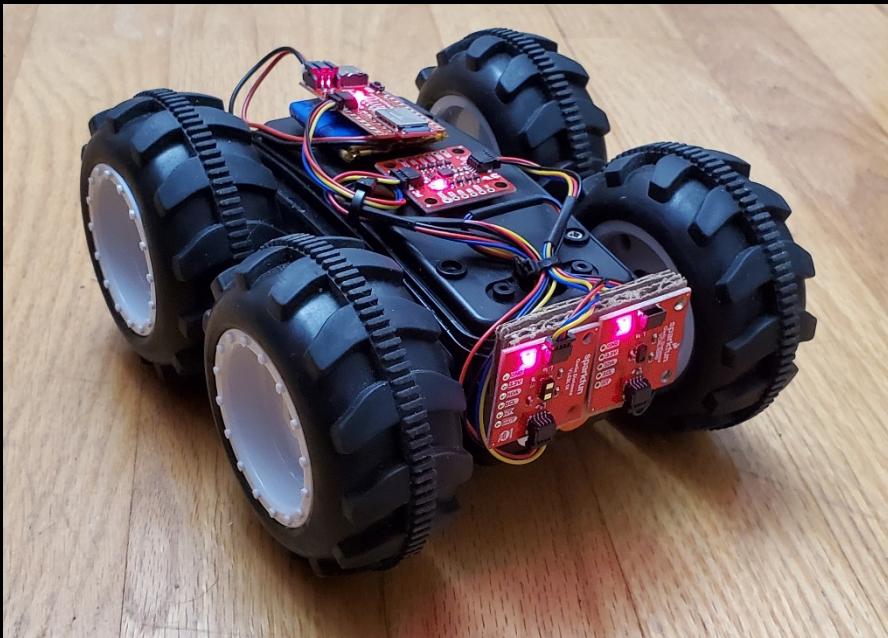
Feedback Control

- Maintain speed prediction at different battery levels



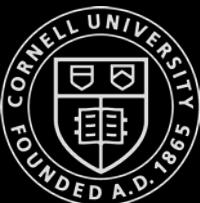
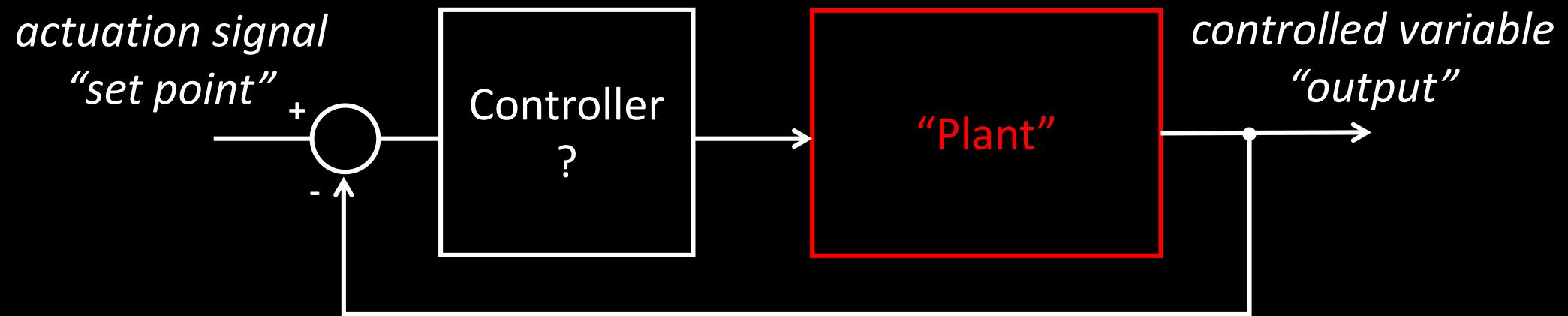
Feedback Control

- Maintaining speed prediction at different battery levels
- Mapping: evenly spaced out sensor readings
- Path execution: adhere to generated path plans



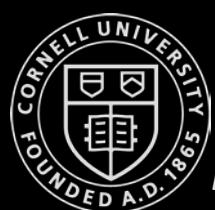
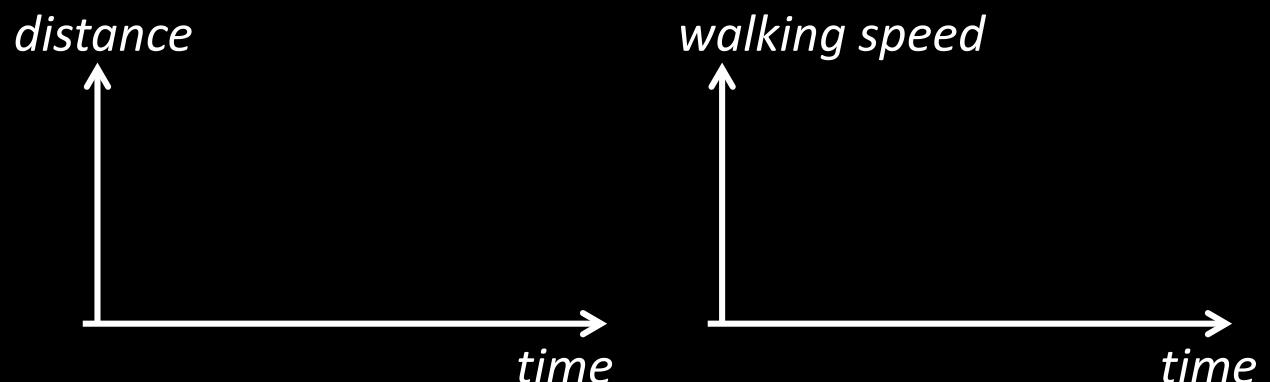
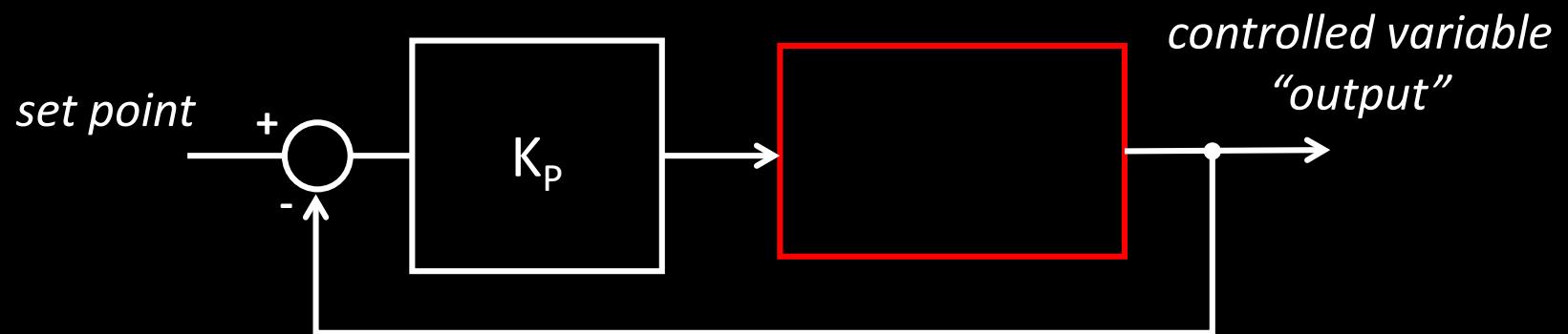
PID control

$$u(t) = K_P e(t) + K_I \int_0^t e(t)dt + K_D \frac{de(t)}{dt}$$



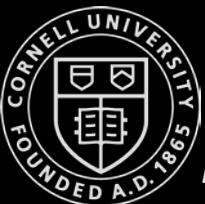
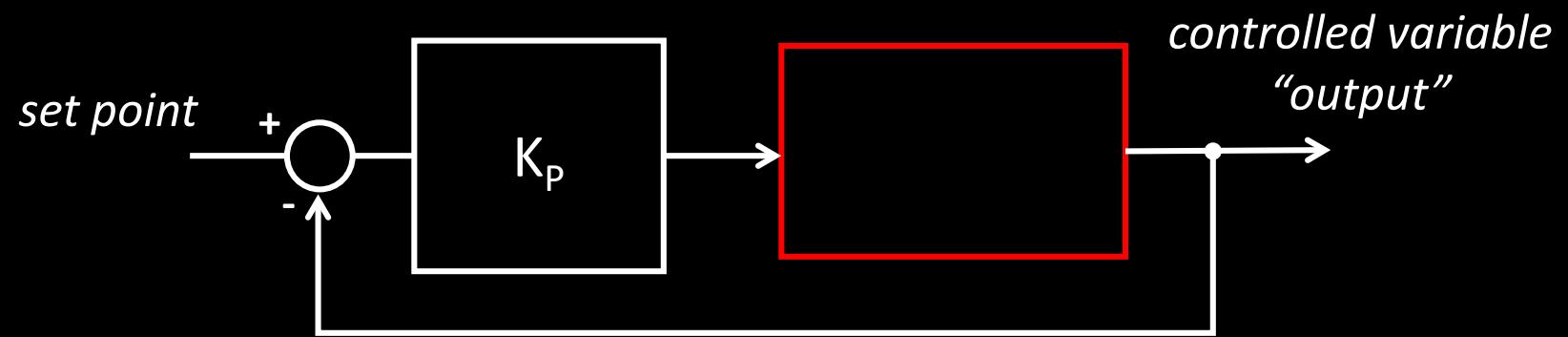
PID control

- Soccer field example



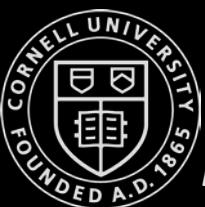
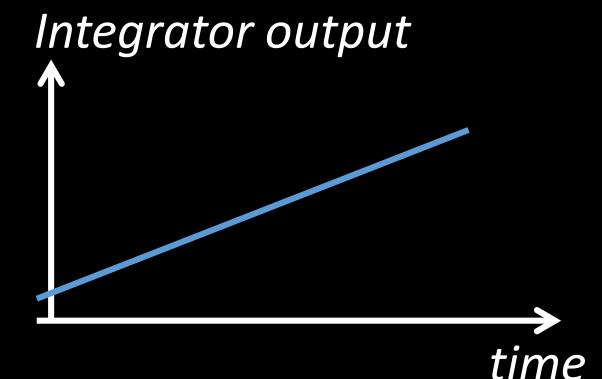
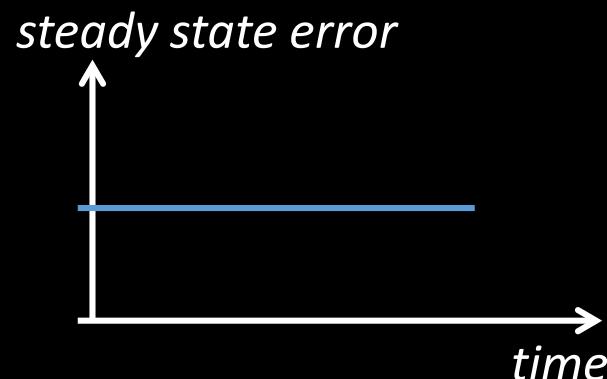
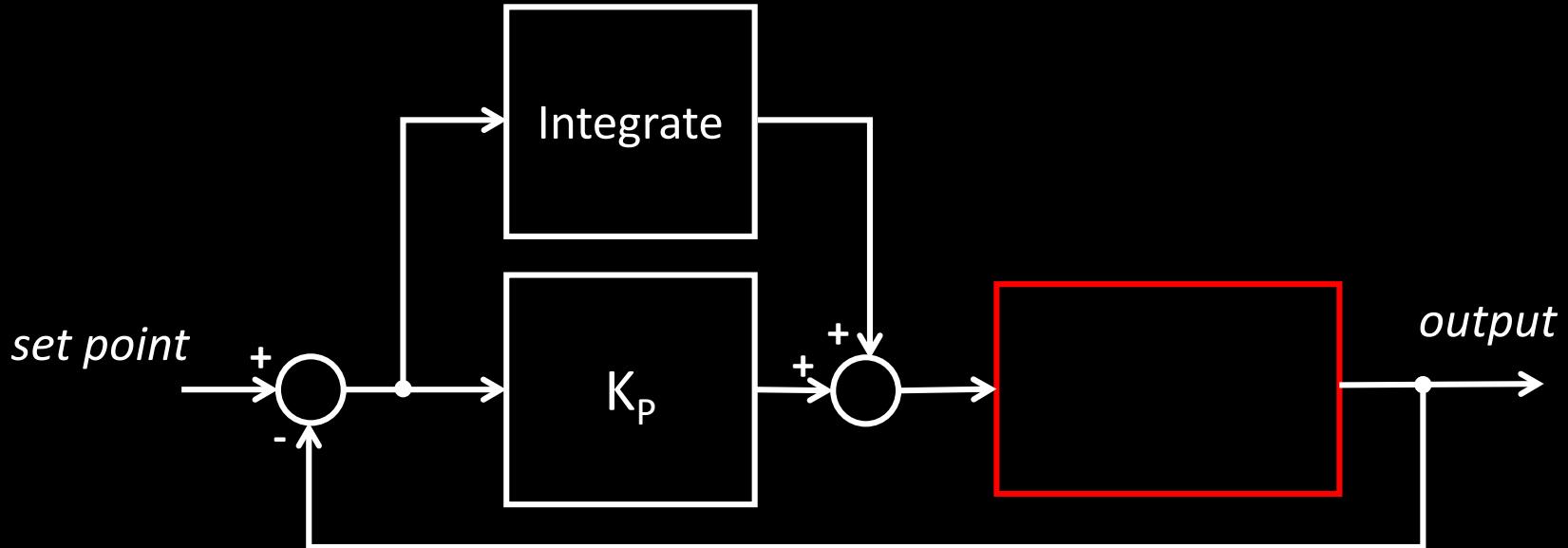
PID control

- Drone example



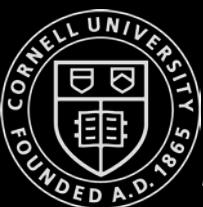
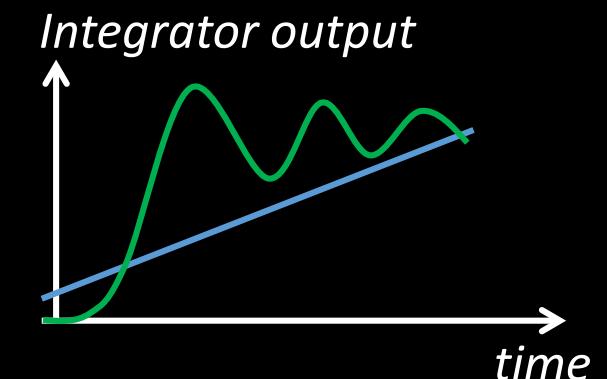
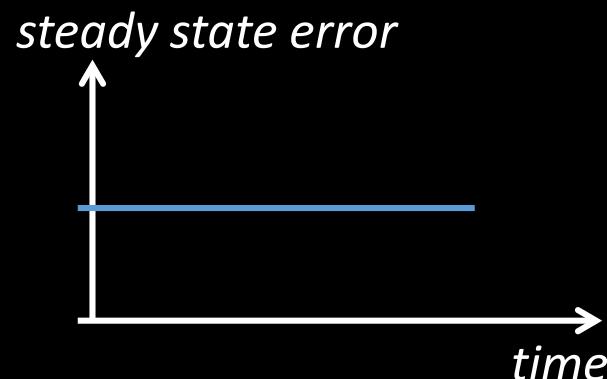
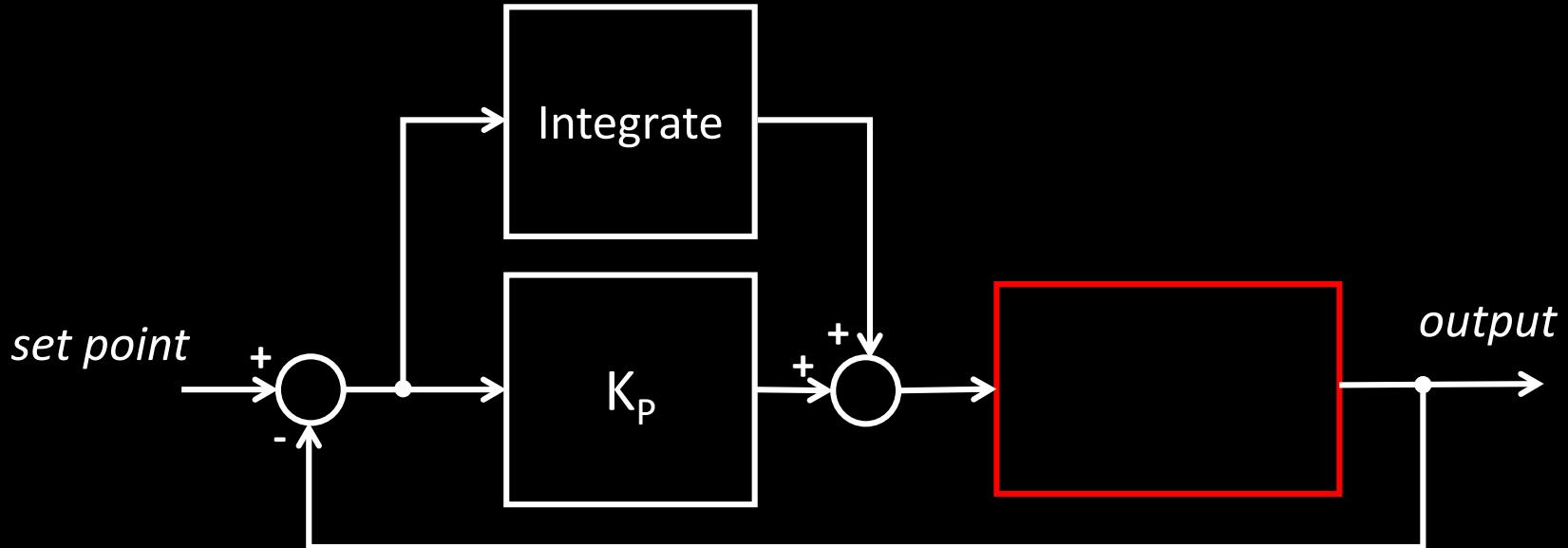
PID control

- Drone example



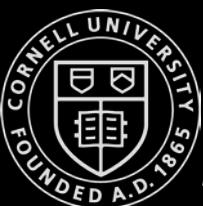
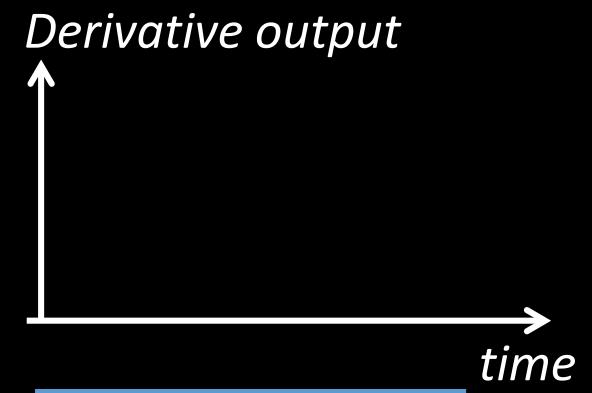
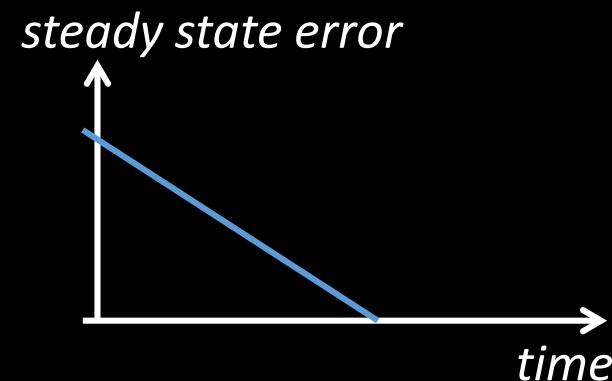
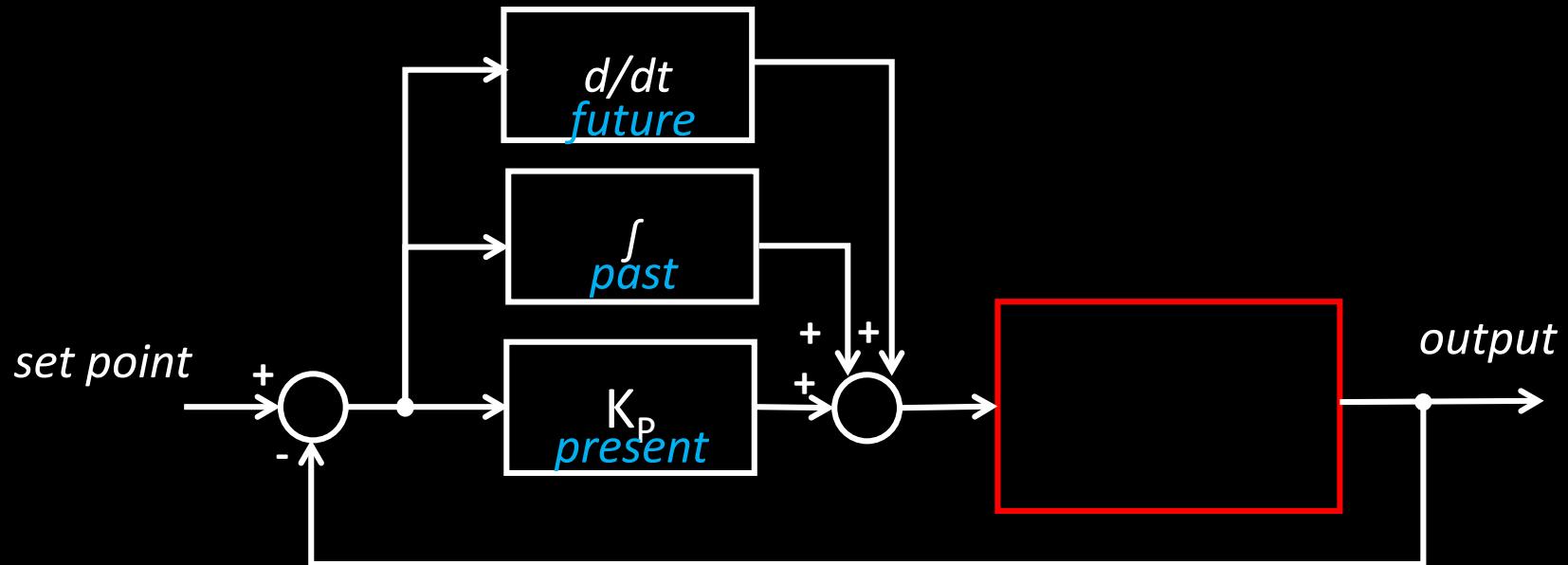
PID control

- Drone example

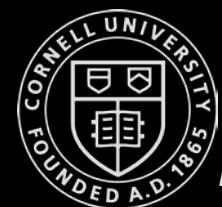
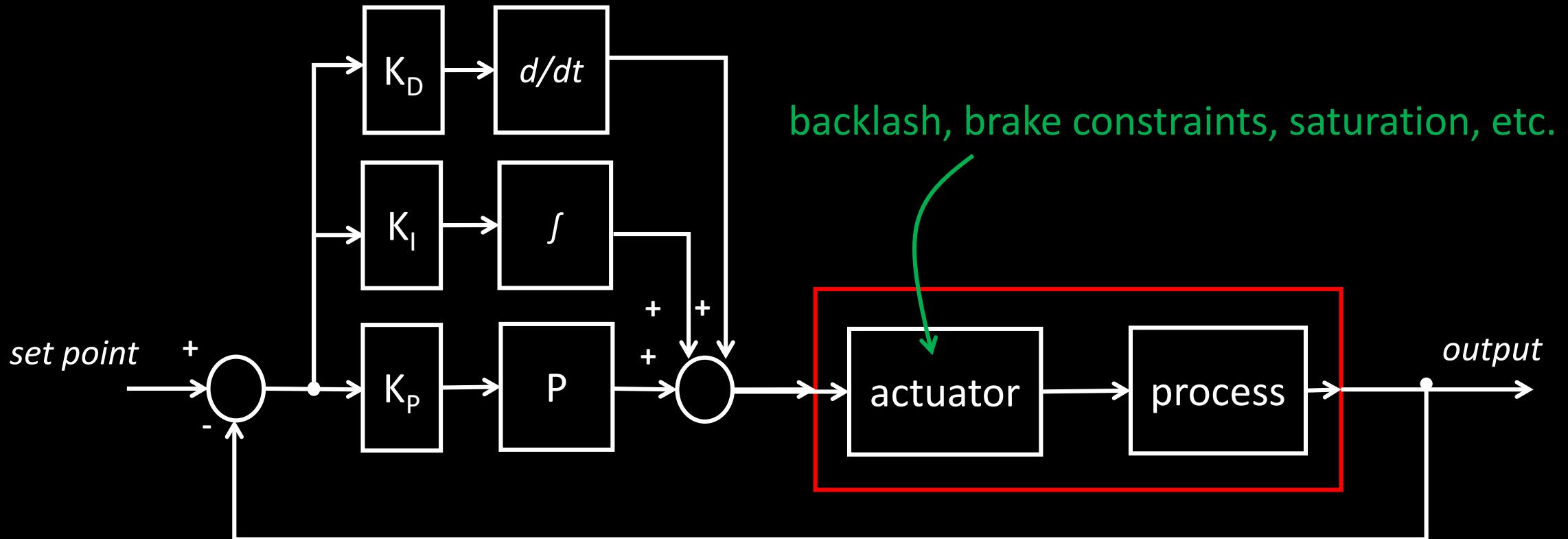


PID control

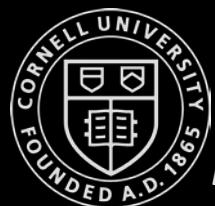
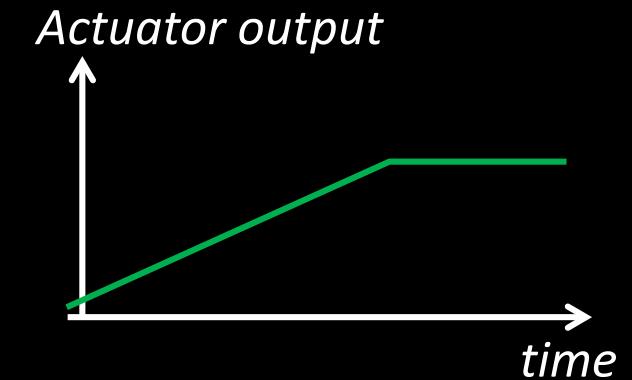
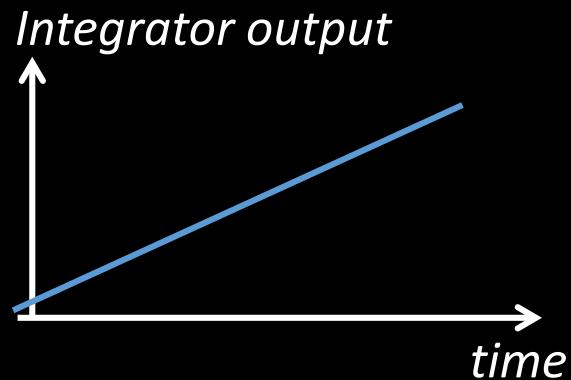
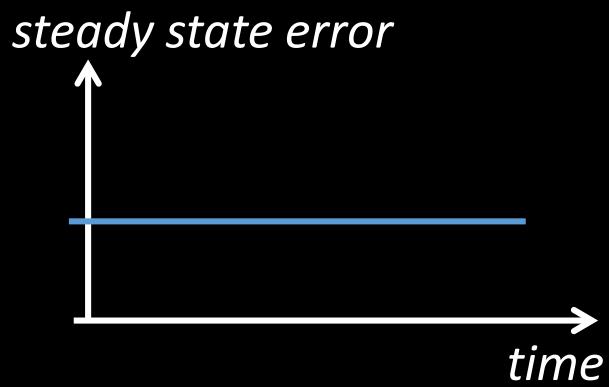
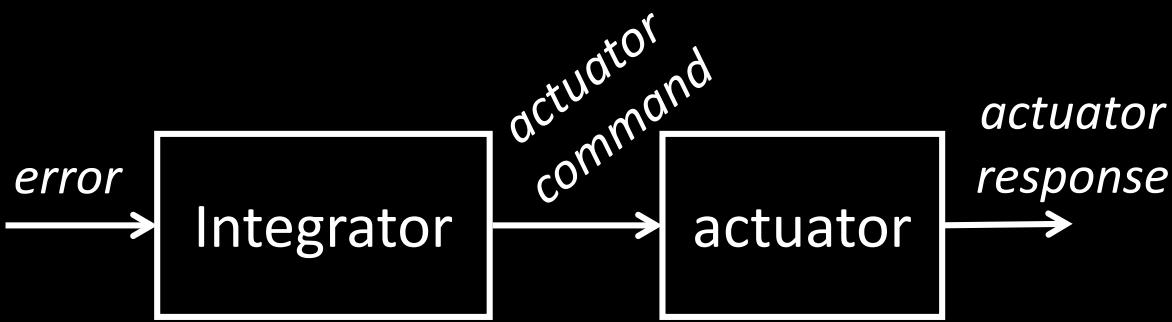
- Drone example



Real Systems are not linear!

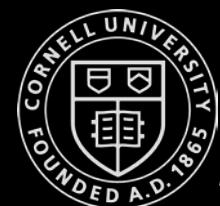
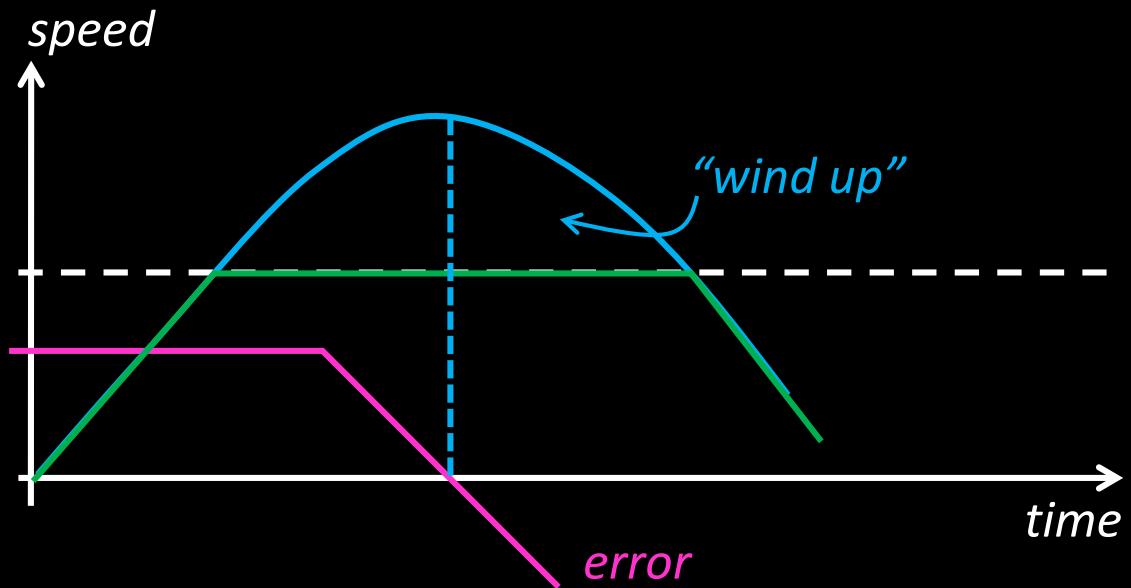
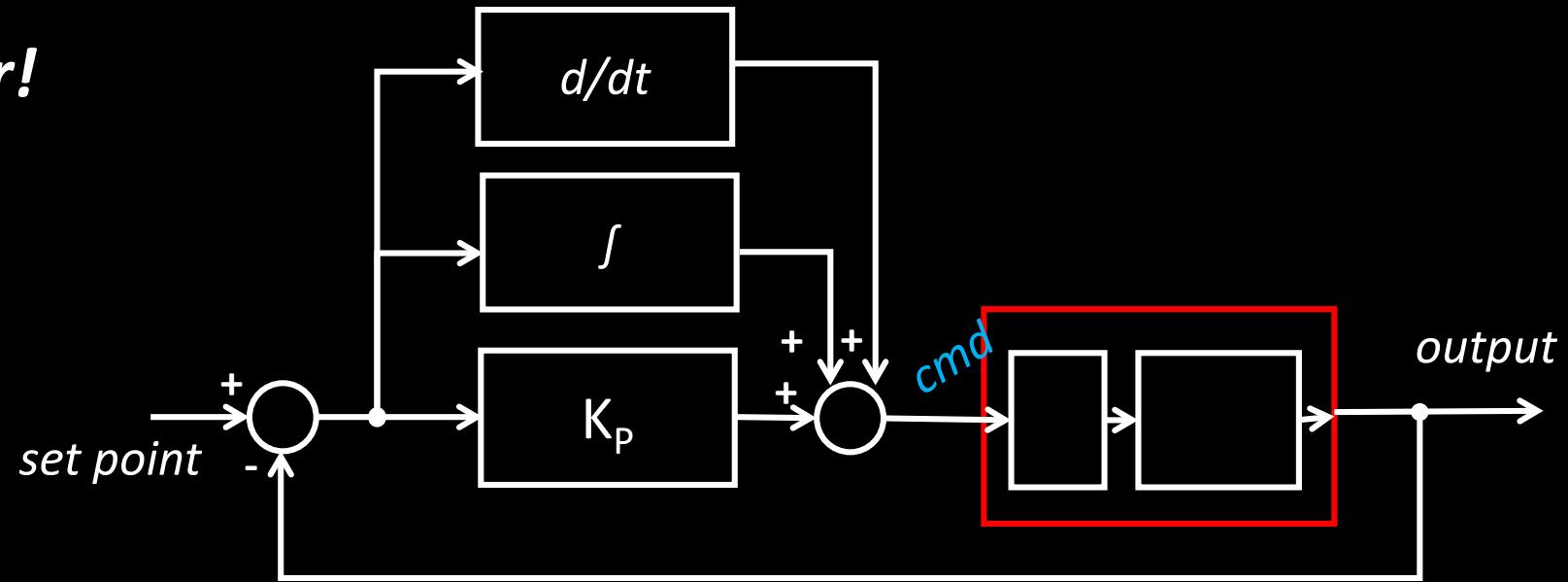


Real Systems are not linear!



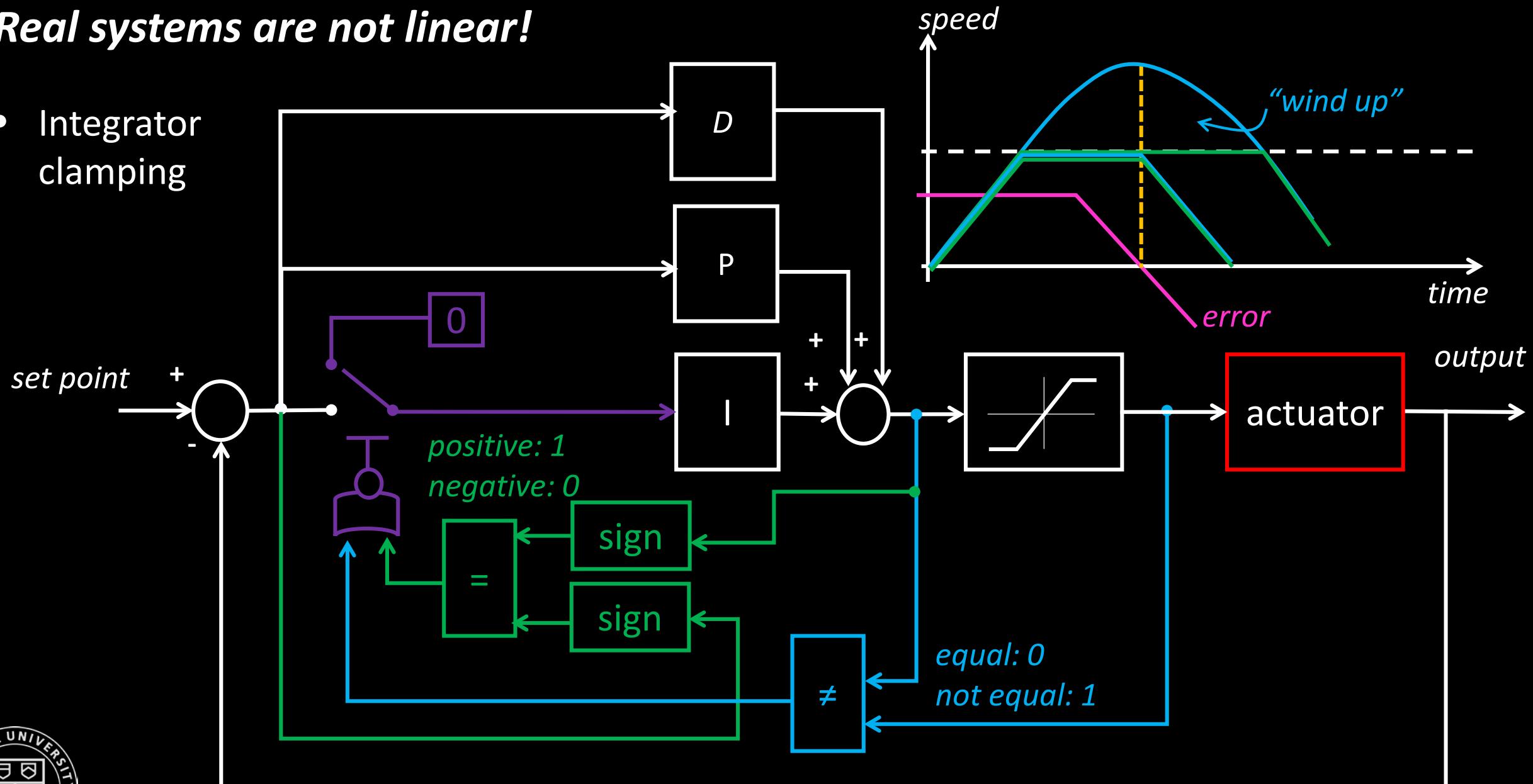
Real systems are not linear!

- Drone example
 - “Integral wind-up”
 - Clamping

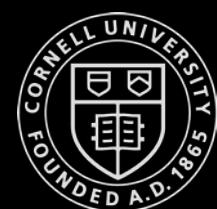
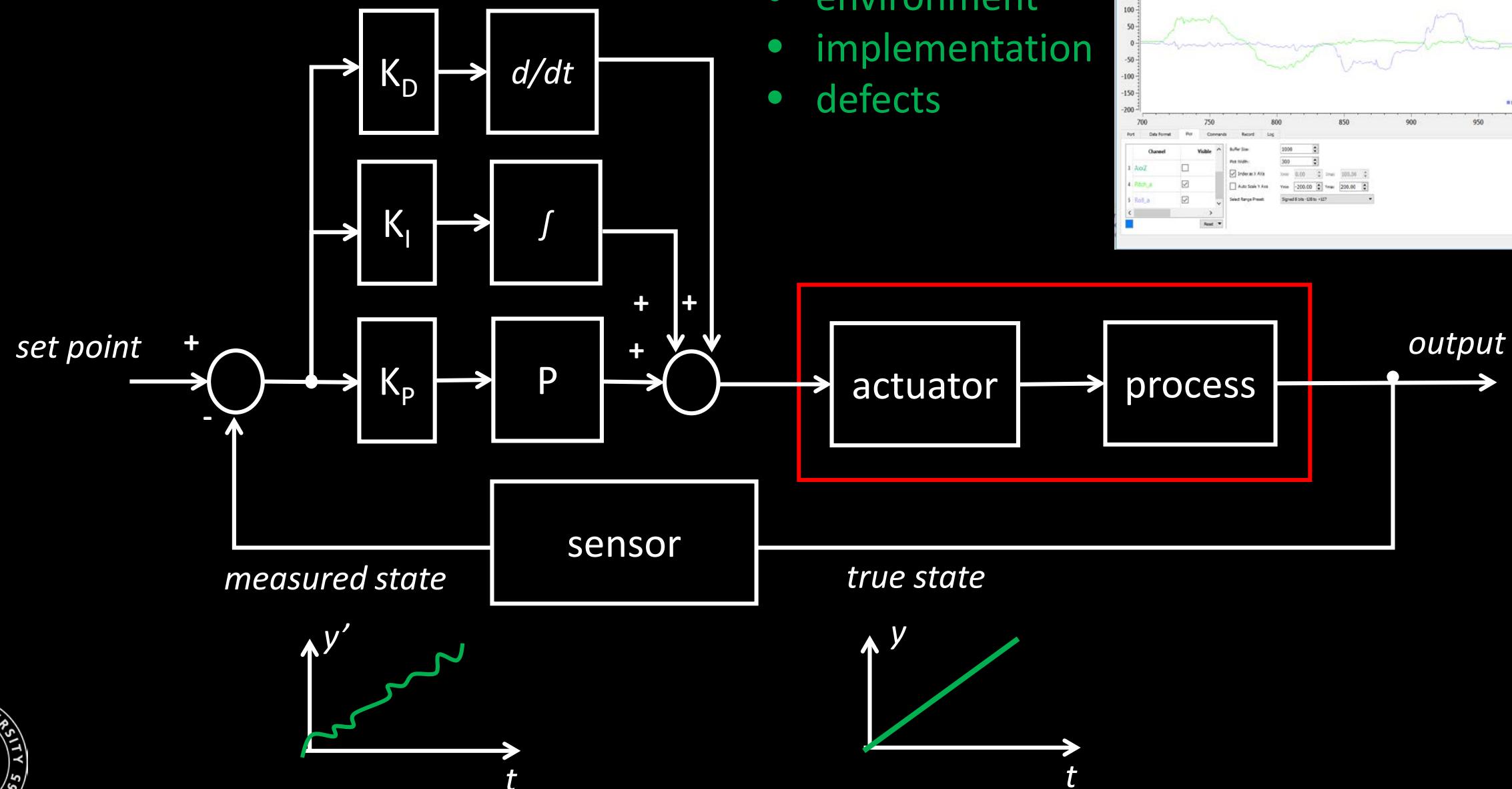


Real systems are not linear!

- Integrator clamping

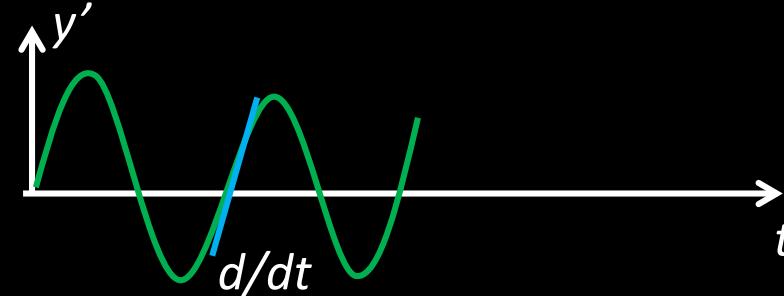
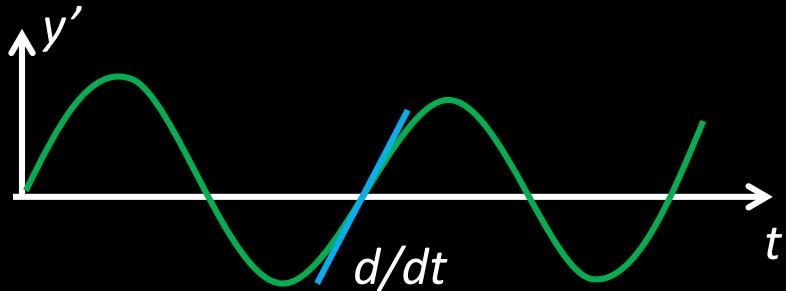


PID and Sensor noise



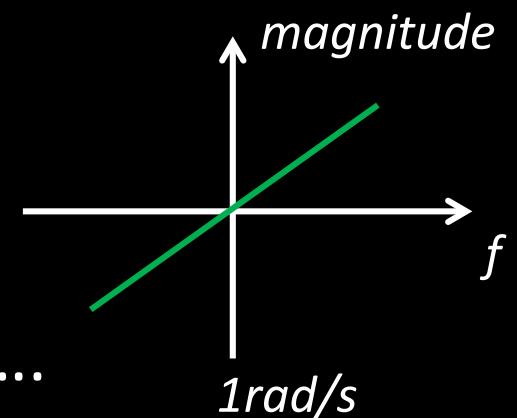
PID and Sensor noise

- Derivatives amplify HF signals more than LF signals

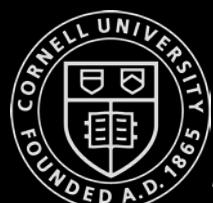


$$y(t) = A\sin(\omega_a t + \phi_a) + B\sin(\omega_b t + \phi_b) + \dots$$

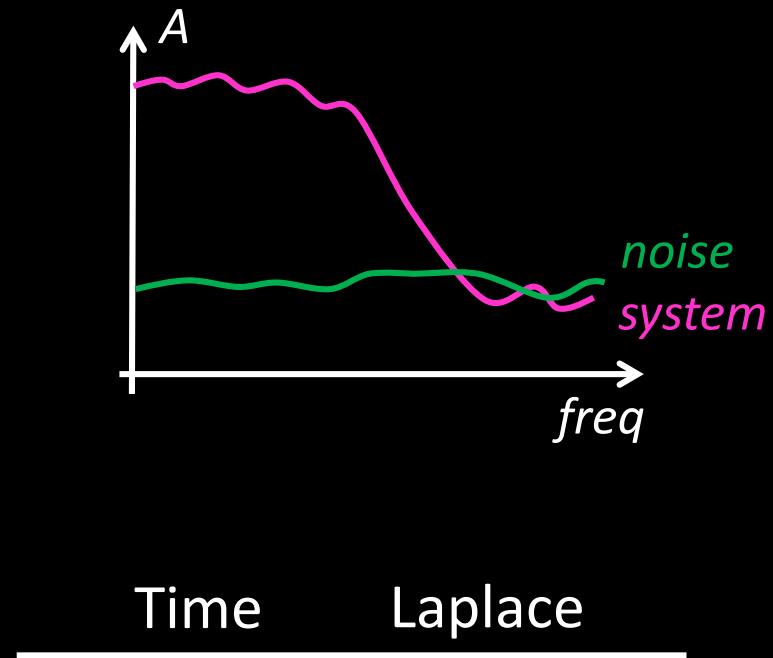
$$dy(t)/dt = A\omega_a \sin(\omega_a t + \phi_a + 90^\circ) + B\omega_b \sin(\omega_b t + \phi_b + 90^\circ) + \dots$$



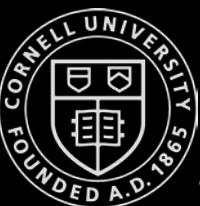
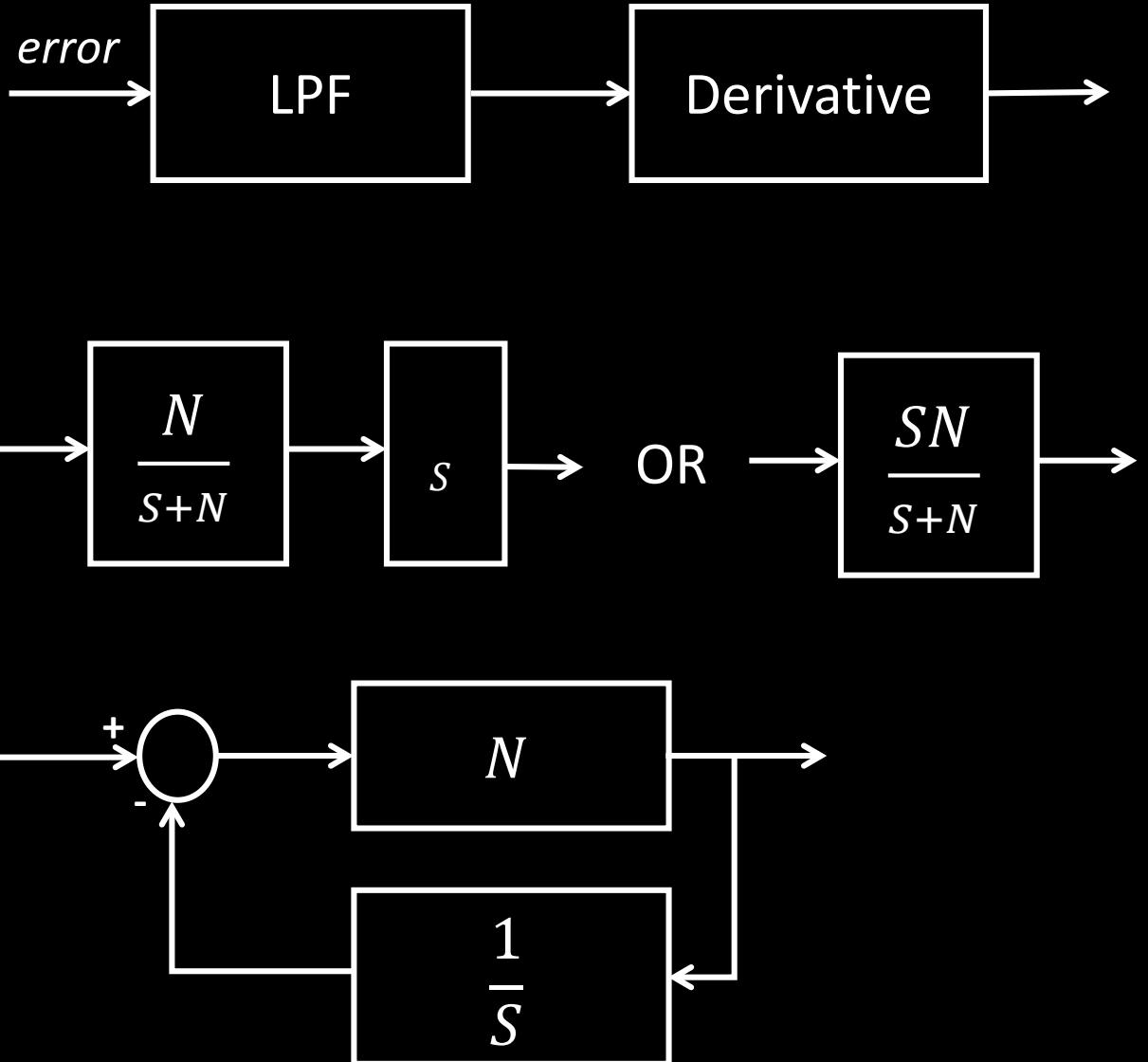
- if $\omega_a > 1\text{rad/s}$, the amplitude will increase
- if $\omega_a < 1\text{rad/s}$, the amplitude will decrease



PID and Sensor noise



$$\begin{array}{ll} \frac{d}{dt} & S \\ \int dt & \frac{1}{S} \\ 1^{\text{st}} \text{ order LPF} & \frac{N}{S+N} = \frac{1}{\frac{1}{N}S+1} = \frac{1}{\tau S + 1} \end{array}$$



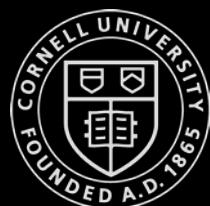
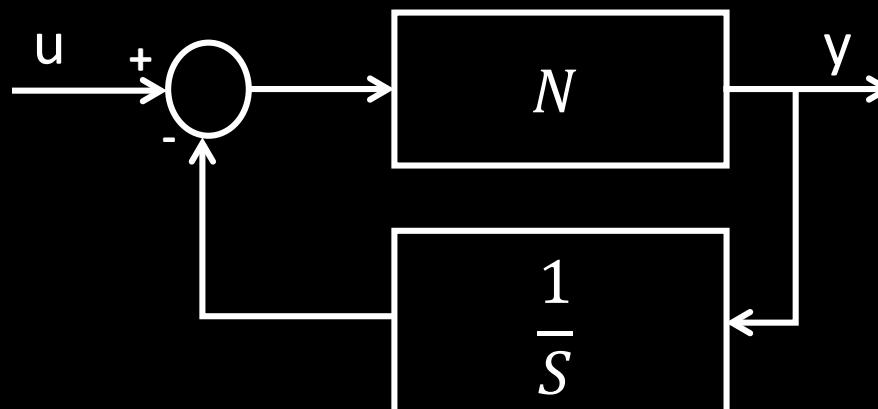
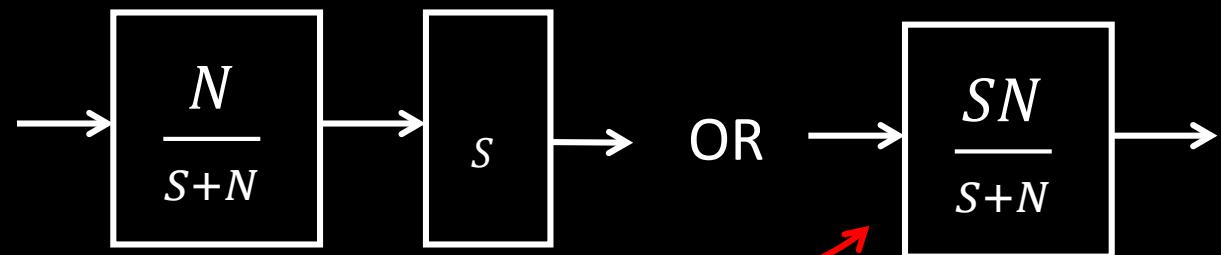
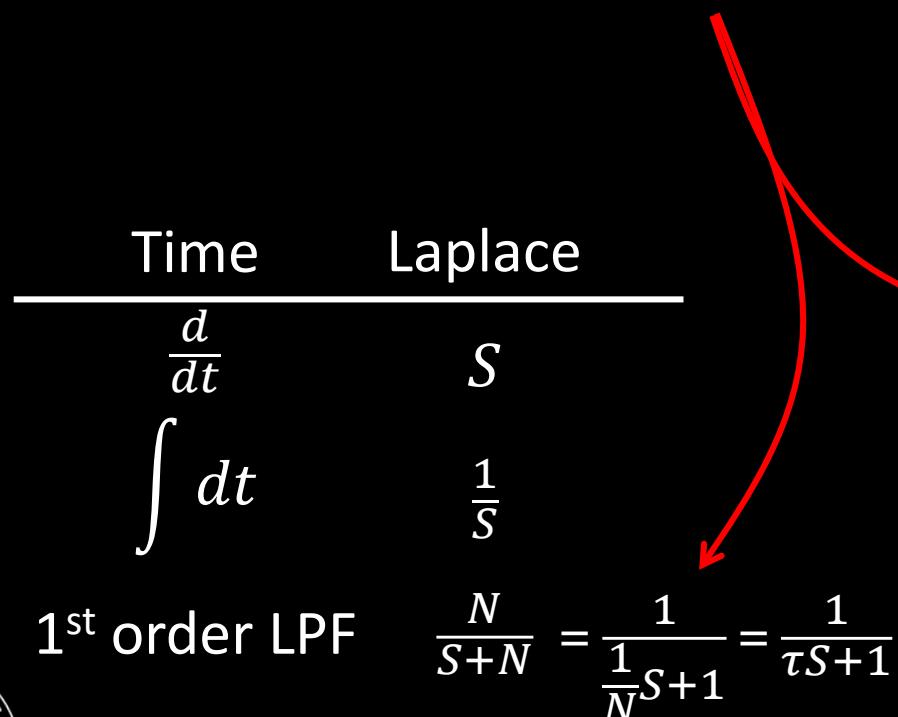
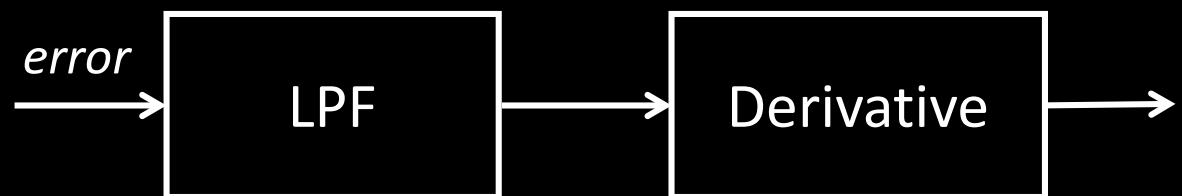
PID and Sensor noise

$$y = N \left(u - \frac{y}{s} \right)$$

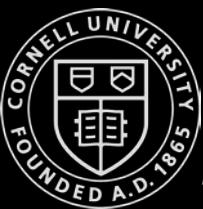
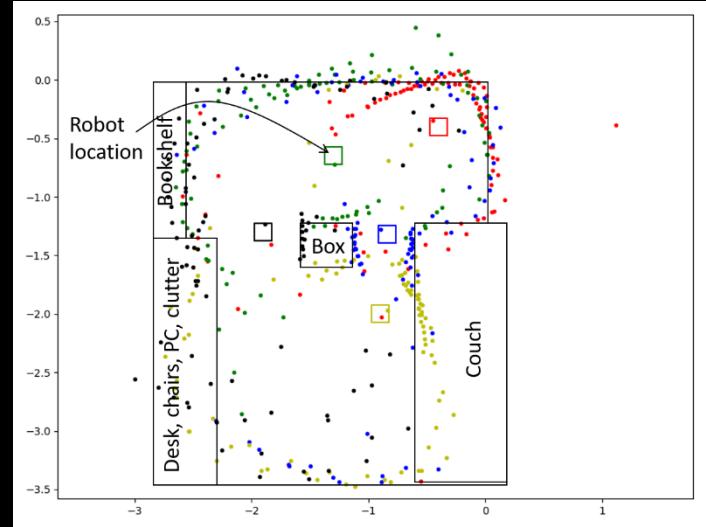
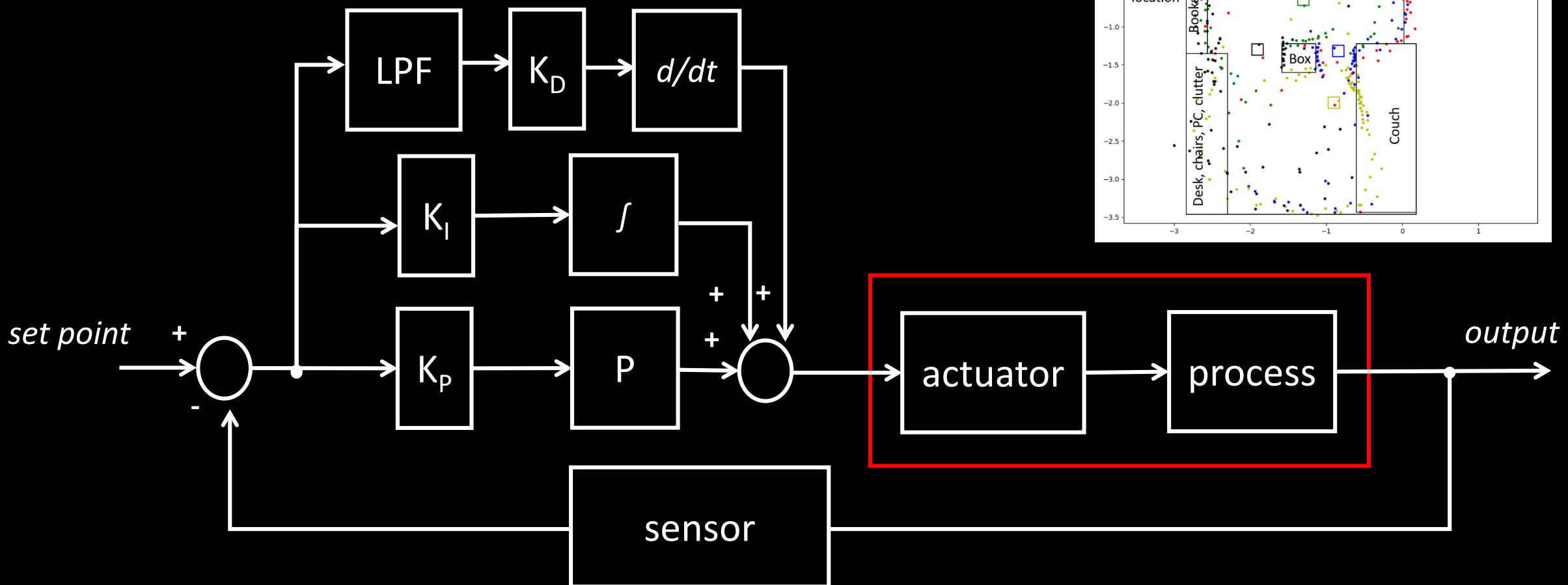
$$y + \frac{Ny}{s} = Nu$$

$$y = \frac{N}{1 + \frac{N}{s}} u$$

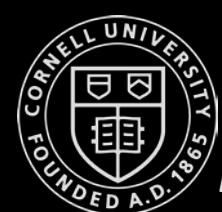
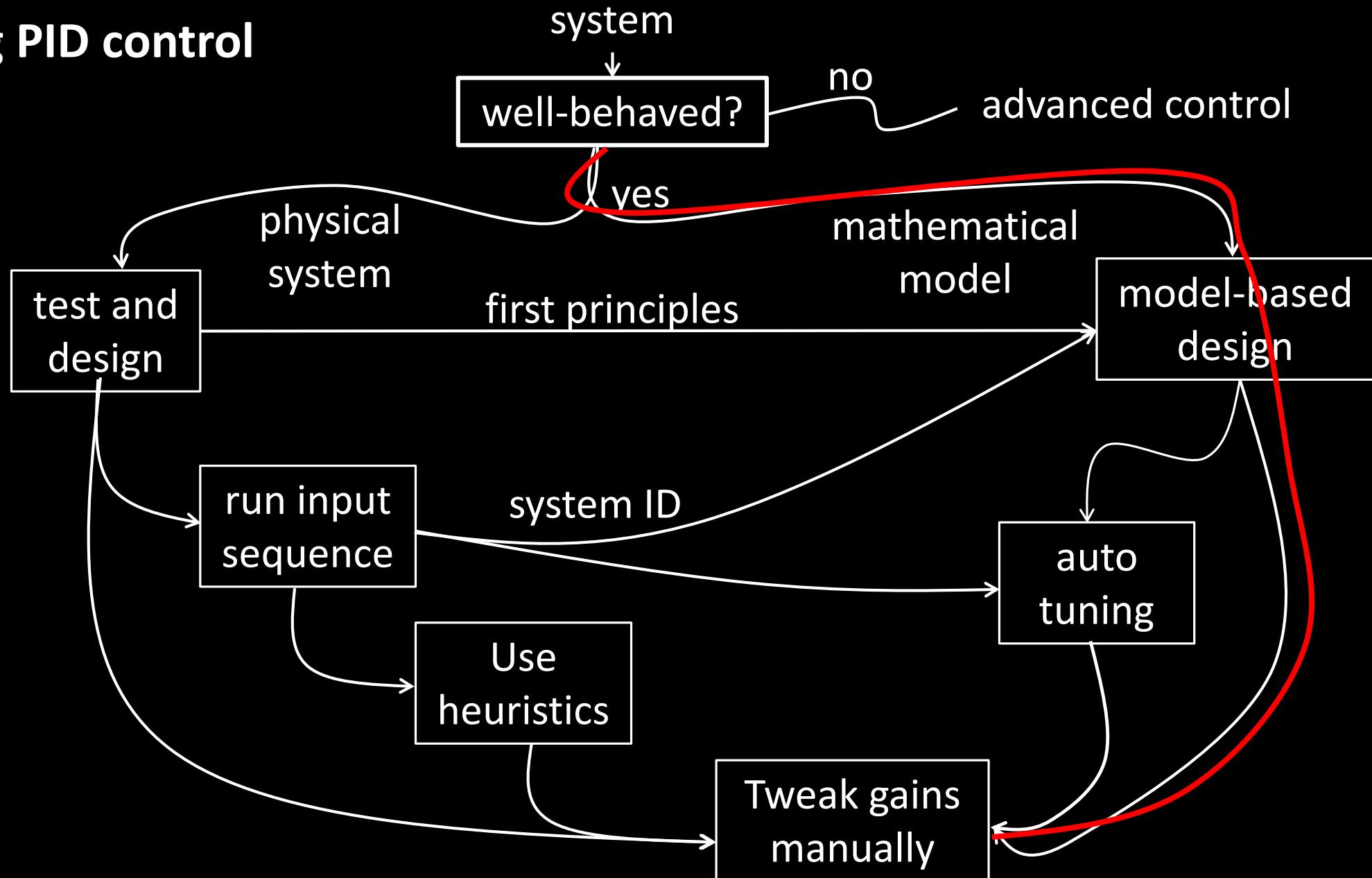
$$\frac{y}{u} = \frac{N}{1 + N\frac{1}{s}}$$



PID

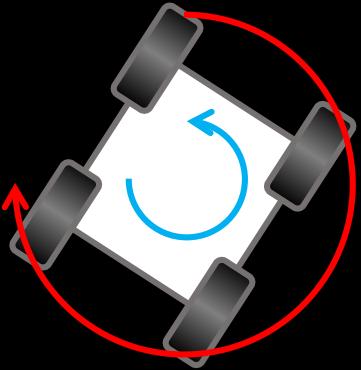


Tuning PID control



Tuning PID control

- PID on turning speed
 - Equations of motion
 - $\dot{x} = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$
 - <https://tinyurl.com/y67glgzk>

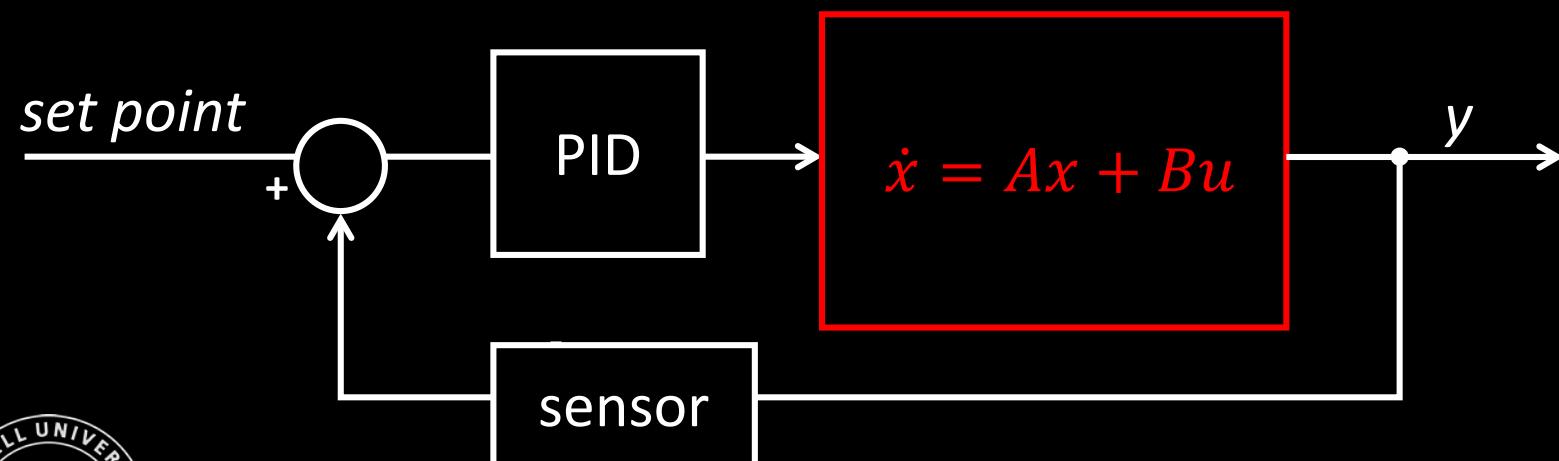


$$F = ma$$

$$\tau = I\alpha$$

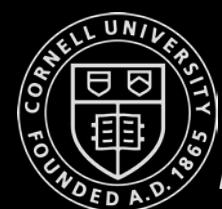
$$\tau = I\ddot{\theta}$$

$$u - \dot{\theta}c = I\ddot{\theta}$$

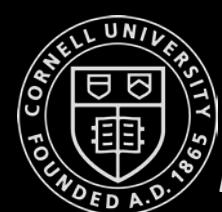
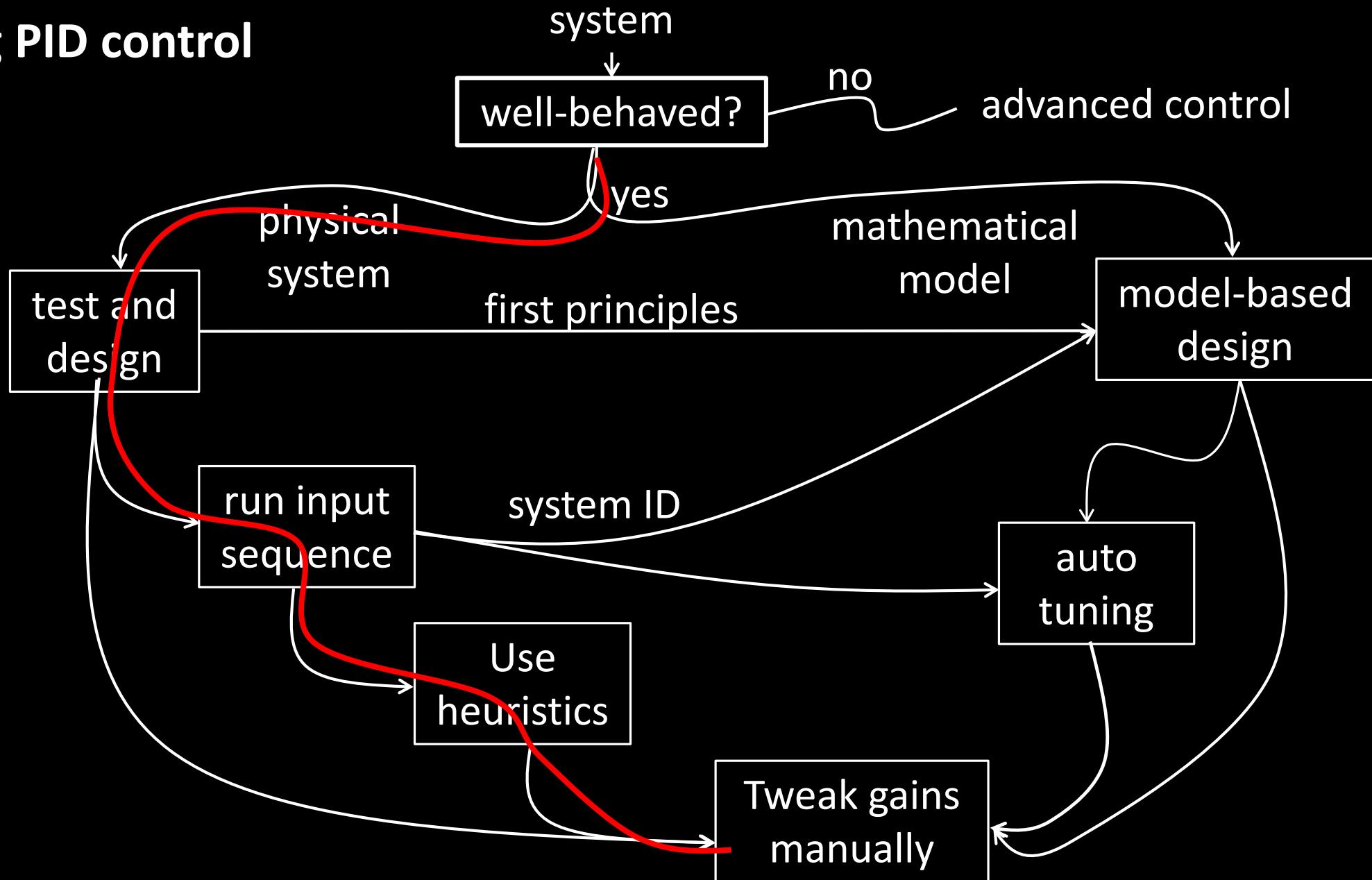


$$\ddot{\theta} = \frac{-\dot{\theta}c}{I} + \frac{1}{I}u$$

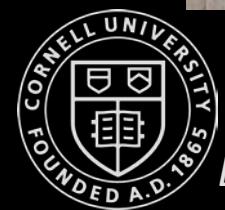
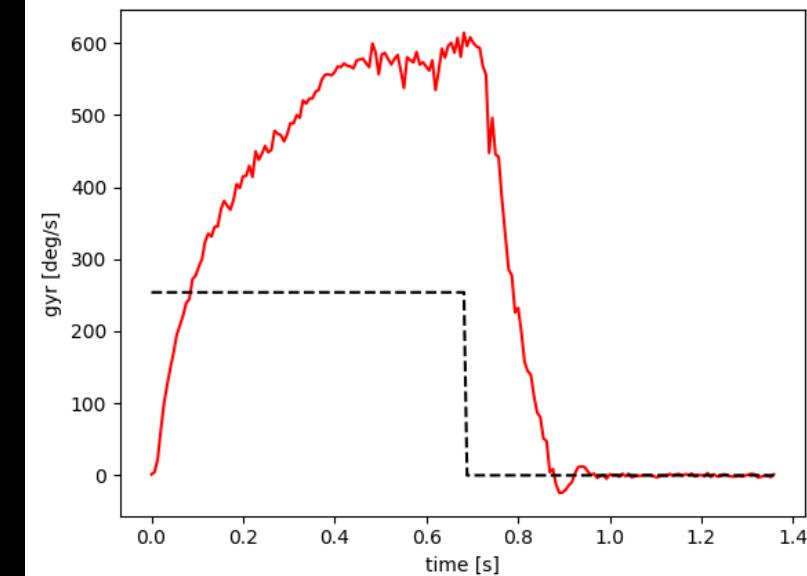
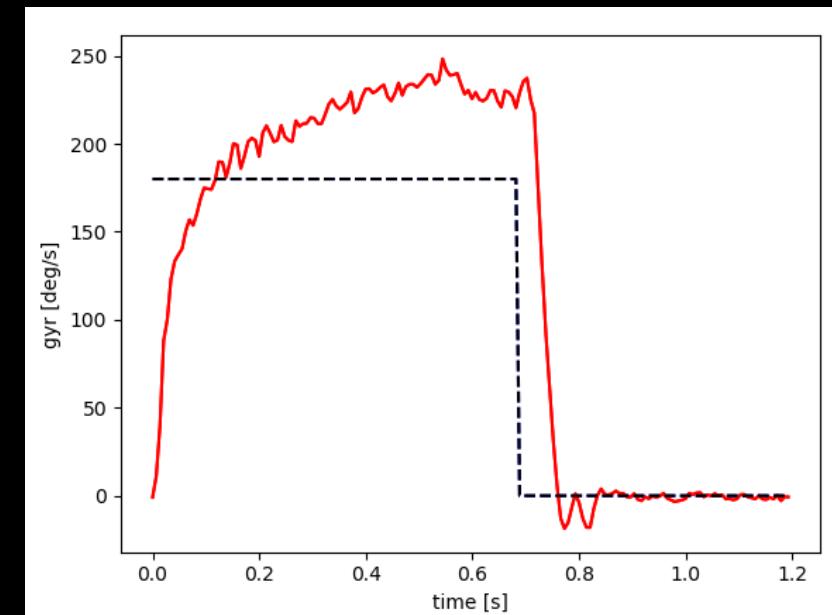
$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & \frac{-c}{I} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{I} \end{bmatrix} u$$



Tuning PID control

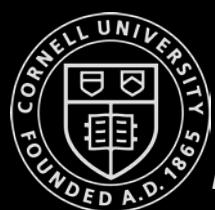
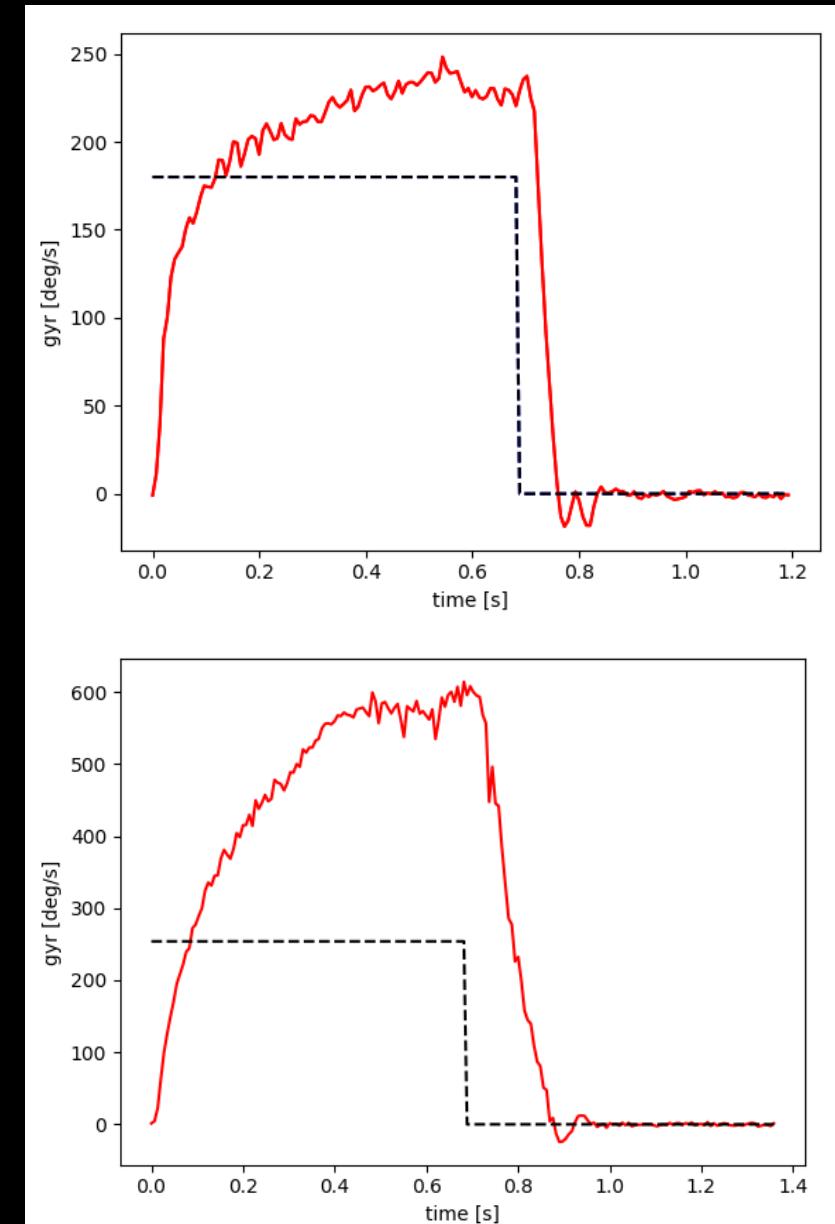
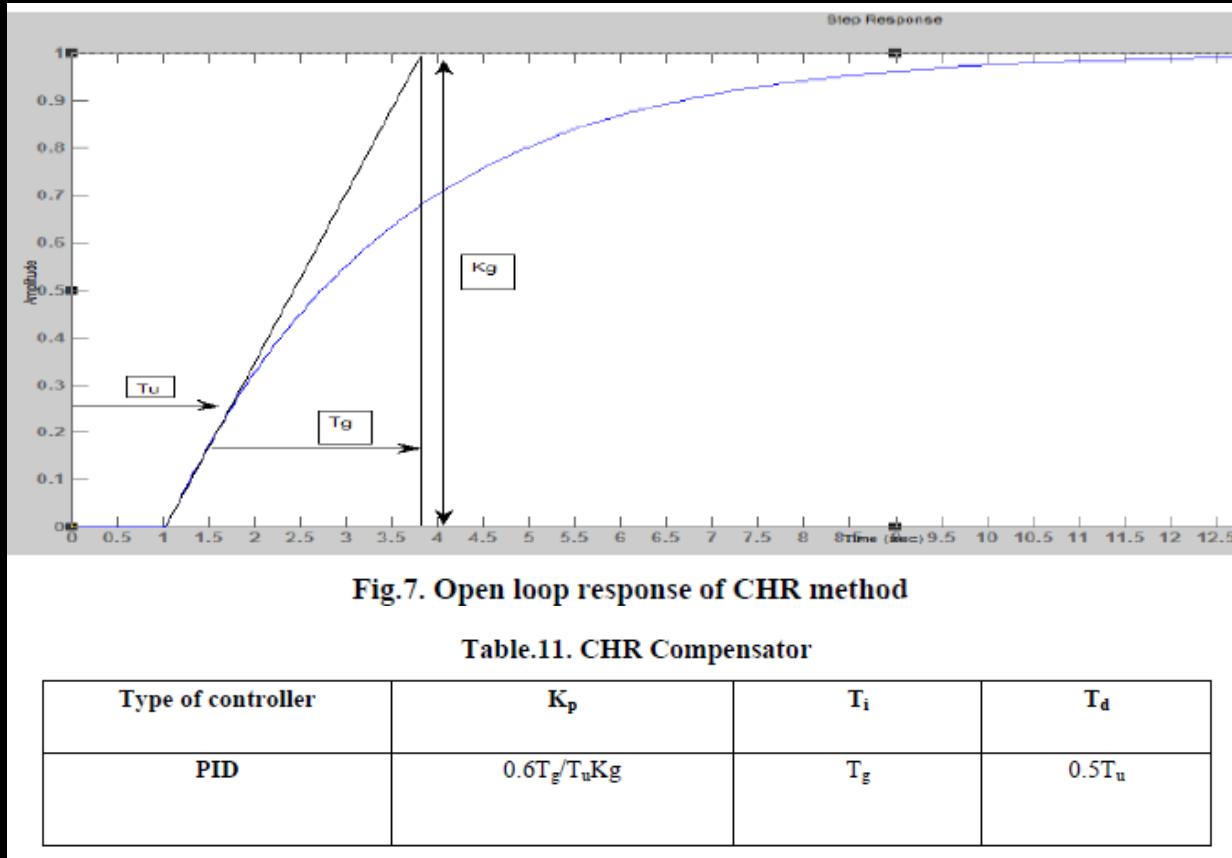


Tuning PID control

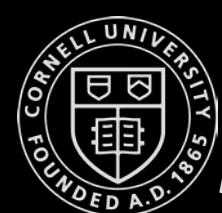
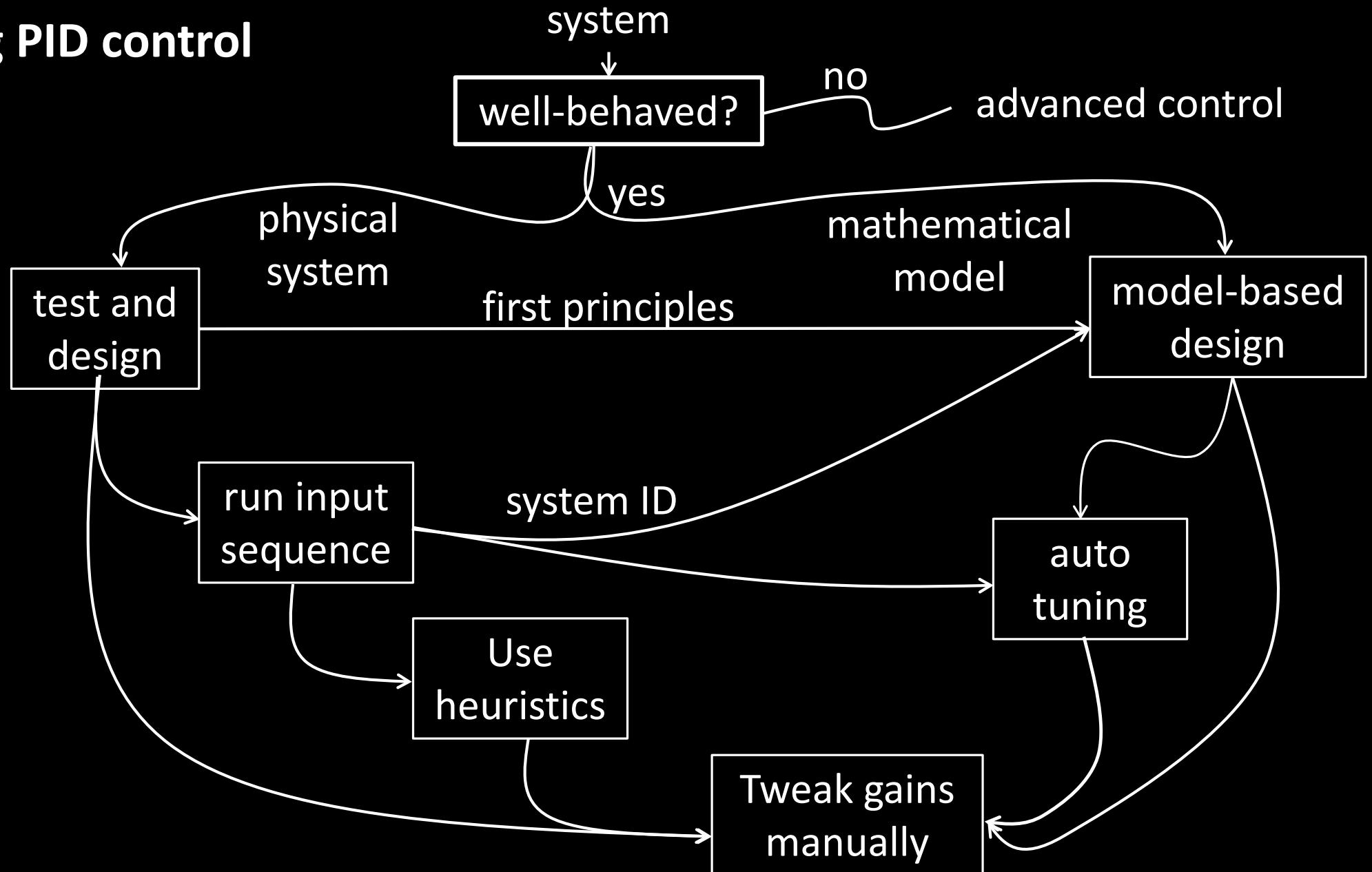


Tuning PID control

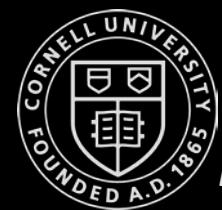
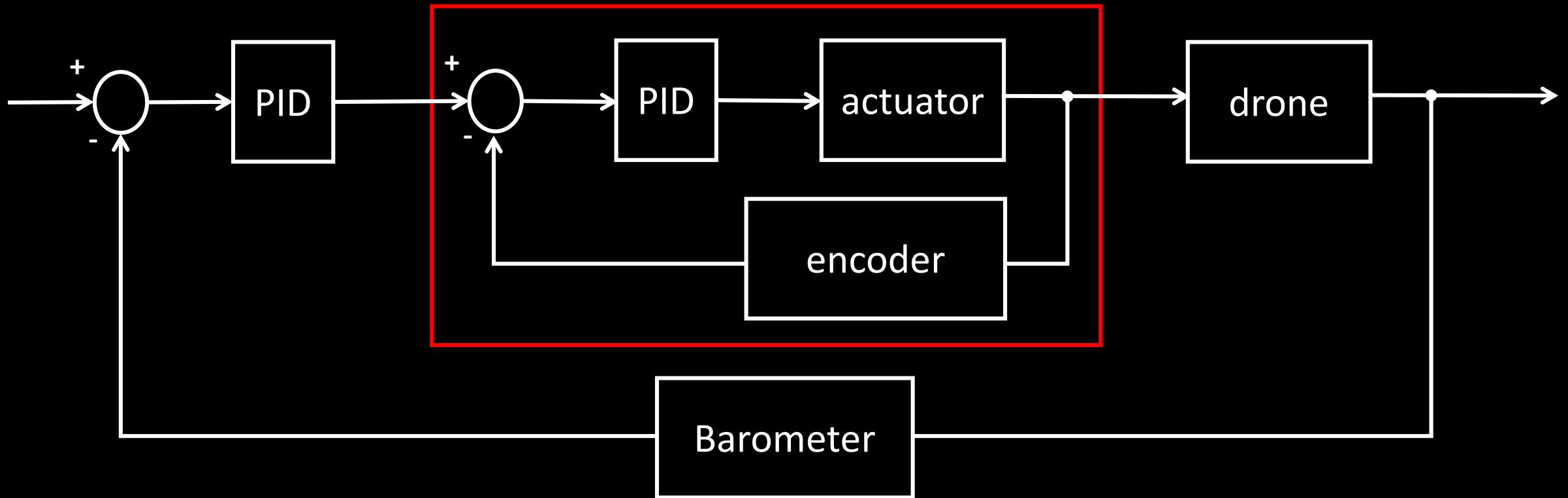
- Chien, Hornes, and Reswick method



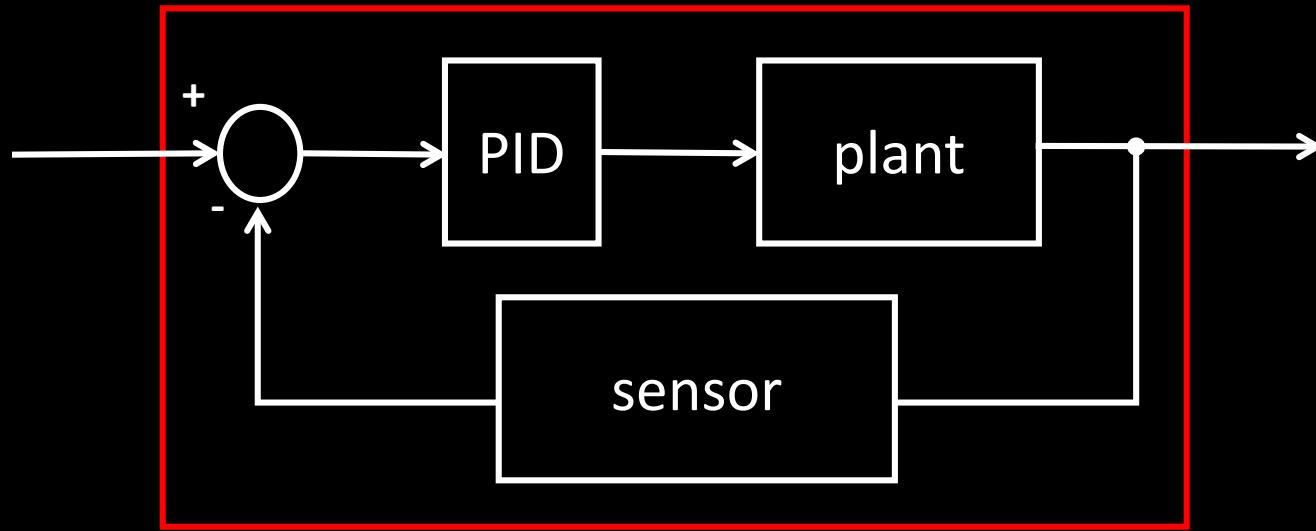
Tuning PID control



Cascaded Control Loops



Discrete PID Control



$$c(s) = K_P + K_I \frac{1}{s} + K_D \frac{N}{1 + N \frac{1}{s}}$$

$$c(z) = K_P + K_I T_s \frac{1}{z - 1} + K_D \frac{N}{1 + N T_s \frac{1}{z - 1}}$$

