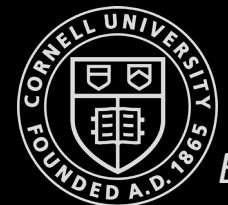
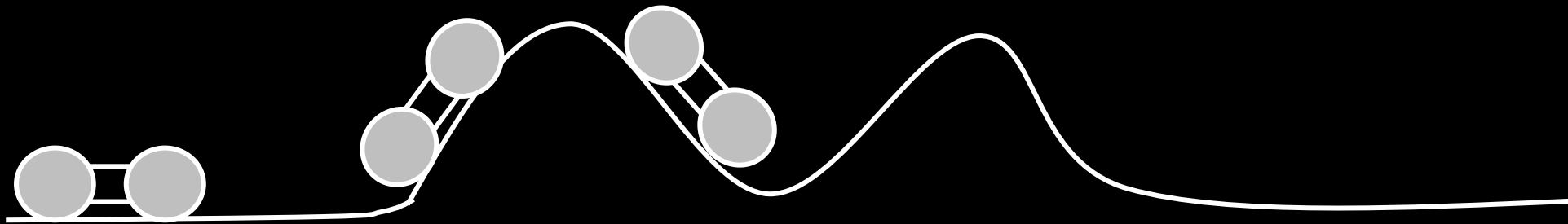


Fast Robots



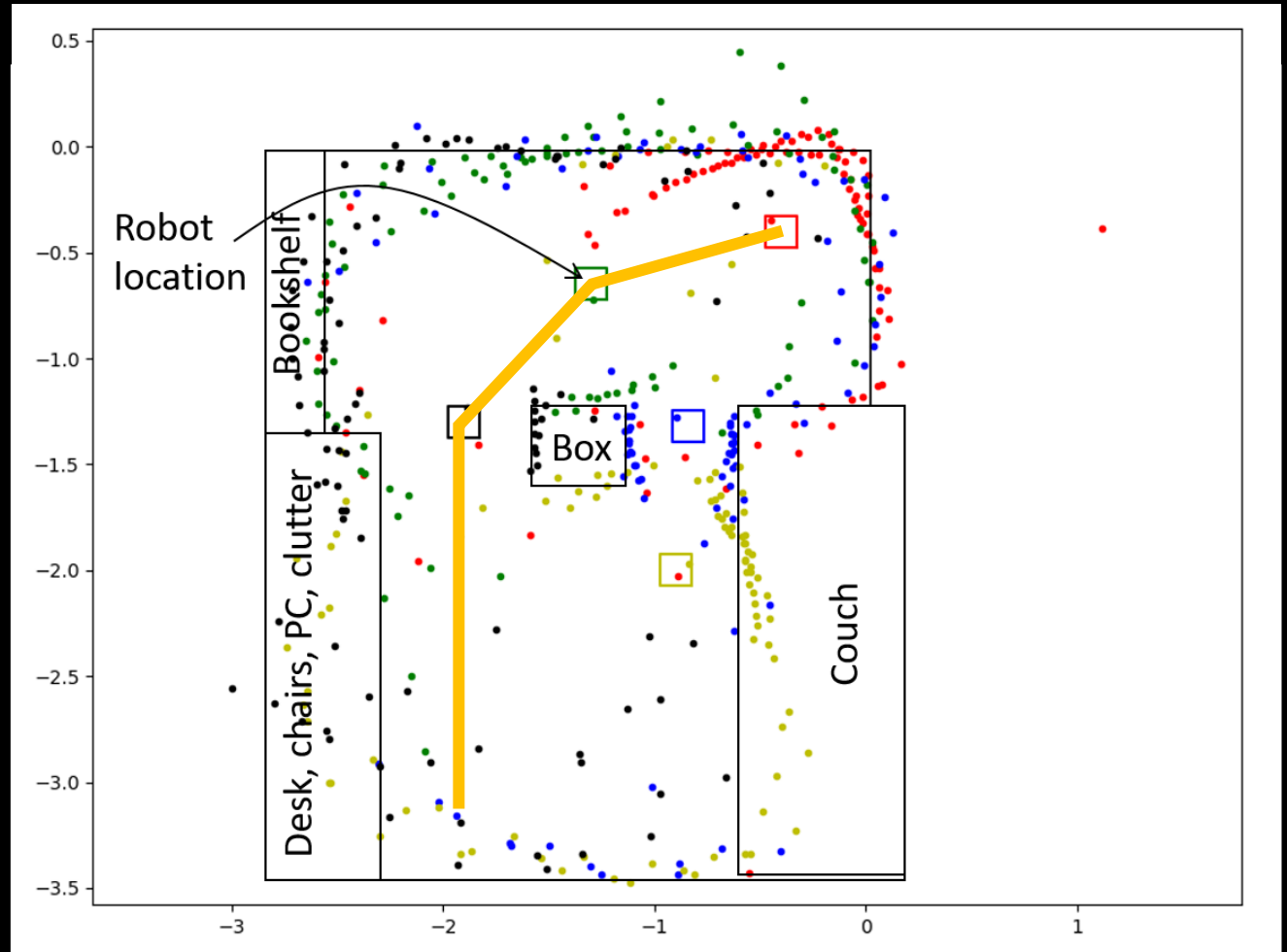
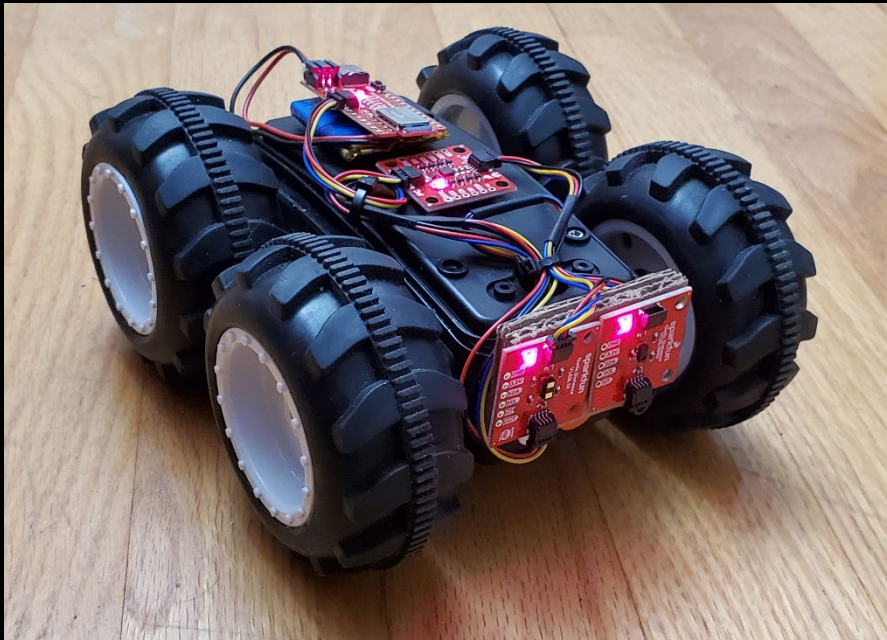
Feedback Control

- Maintaining speed prediction at different battery levels, over different surfaces
- Maintaining position with respect to walls
- Etc.



Feedback Control

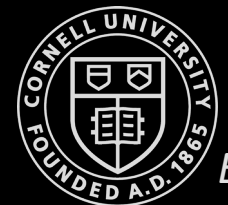
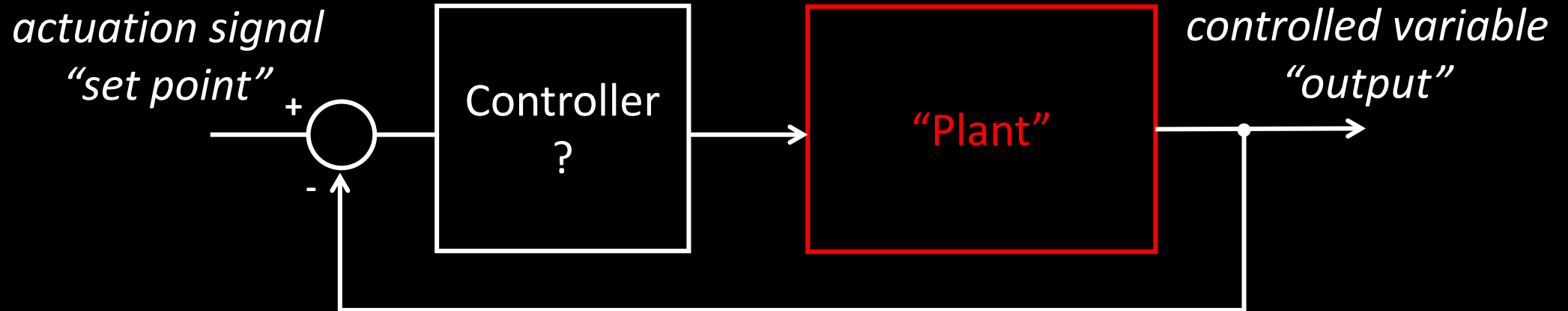
- Maintaining speed prediction at different battery levels and over different surfaces
- Mapping: evenly spaced out sensor readings
- Path execution: adhere to generated path plans



PID control

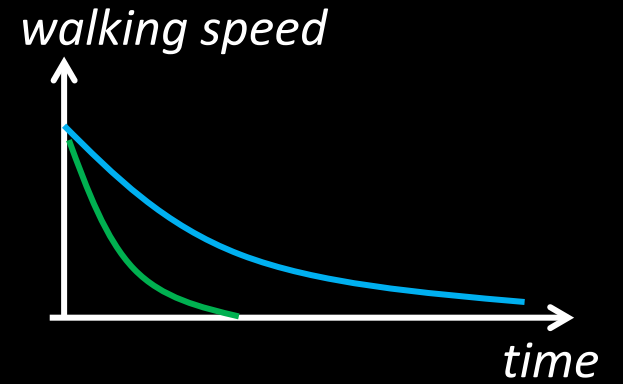
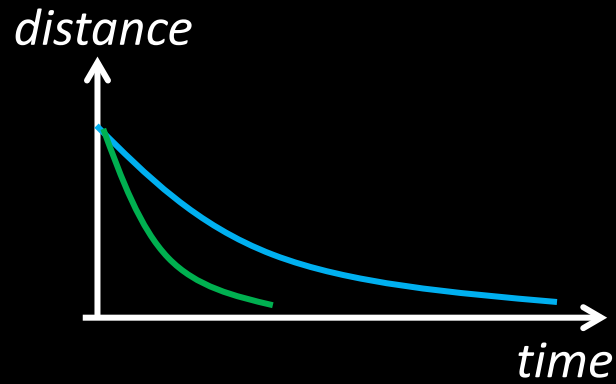
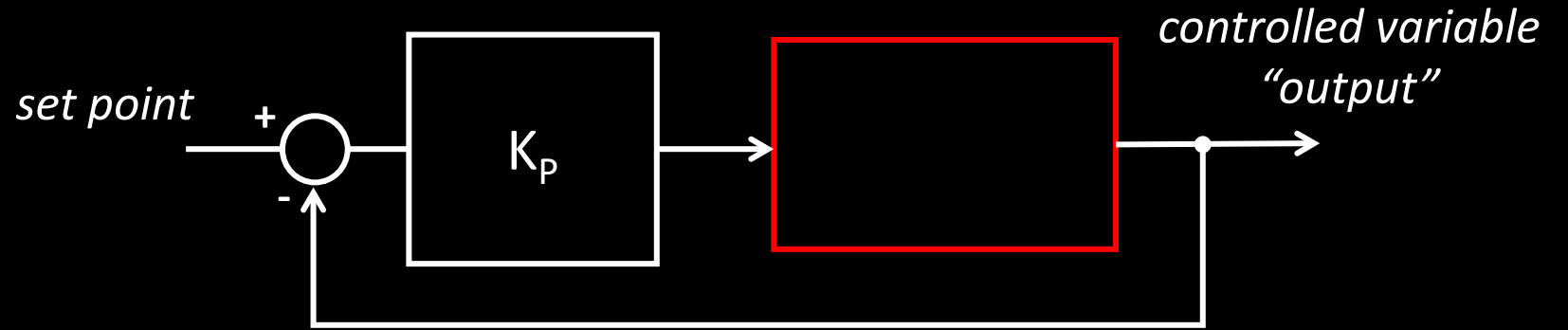
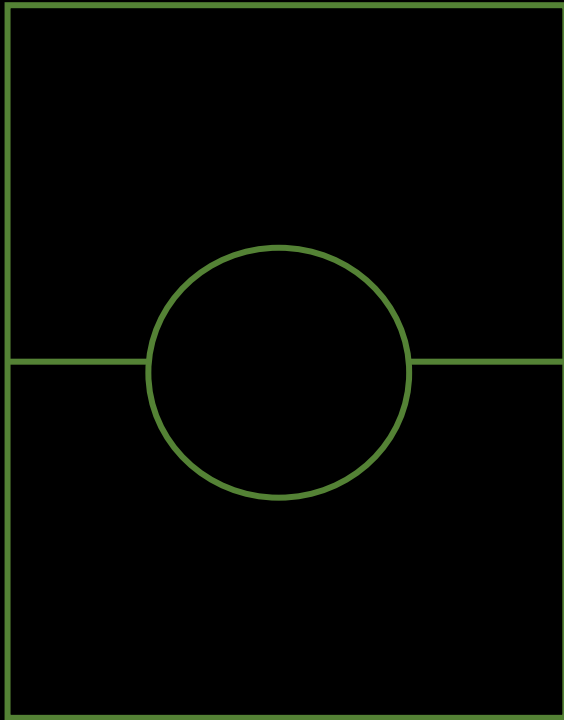
*Heavily inspired by a
Matlab Tech Talk:
Understanding PID Control*

$$u(t) = K_P e(t) + K_I \int_0^t e(t) dt + K_D \frac{de(t)}{dt}$$



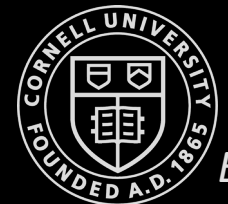
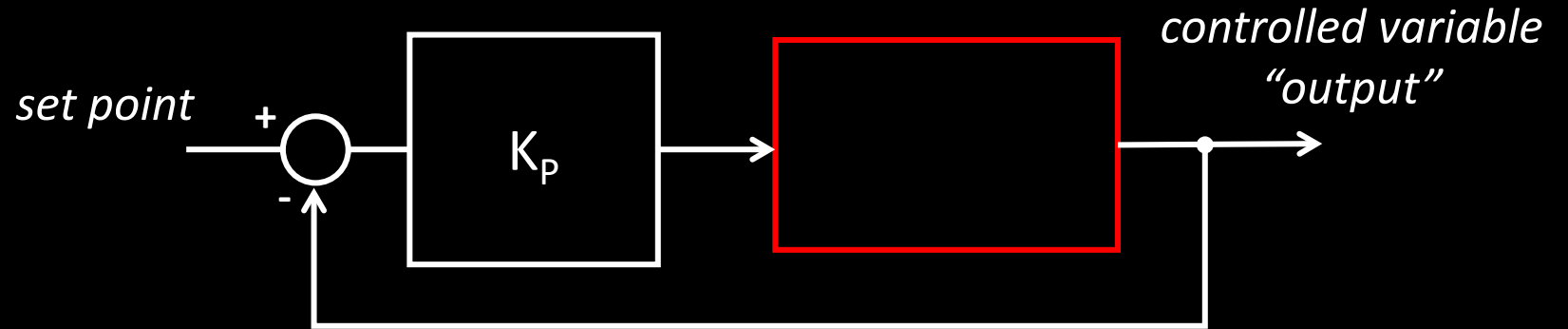
PID control

- Soccer field example



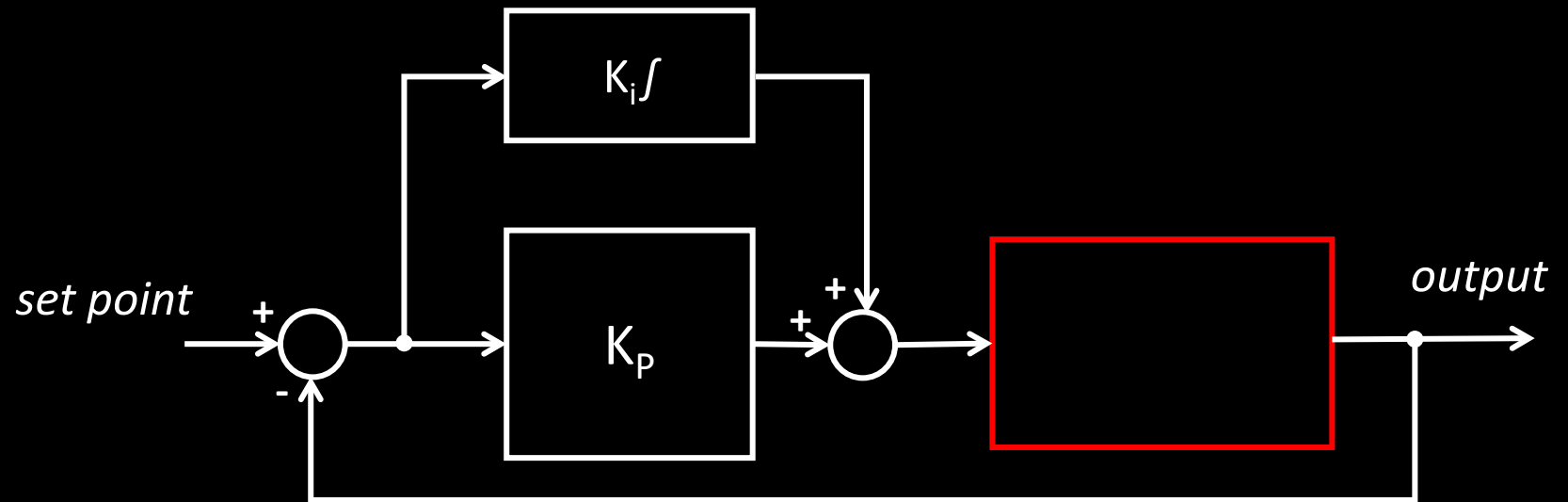
PID control

- Drone example
 - But there's gravity...
 - Hover at 100rpm
 - $K_p = 2, a > 0m$
 - $K_p = 5, a = 30m$
 - $K_p = 10, a = 40m$
 - $K_p = 100, a = 49m$
 - Steady state error

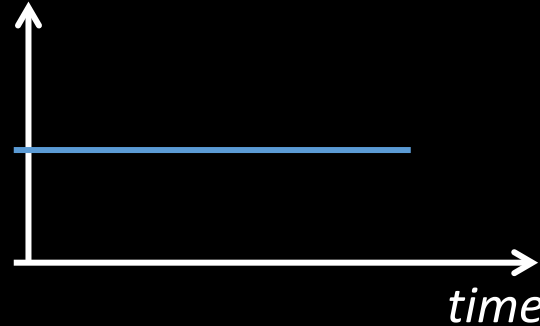


PID control

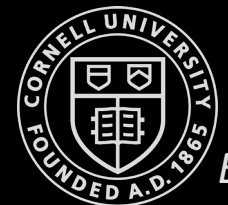
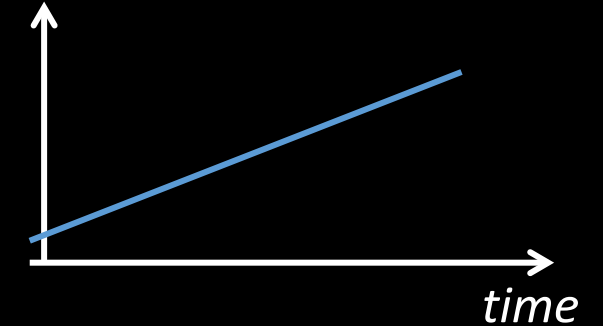
- Drone example
 - But there's gravity...
 - Hover at 100rpm
 - $K_p = 2, a > 0m$



steady state error

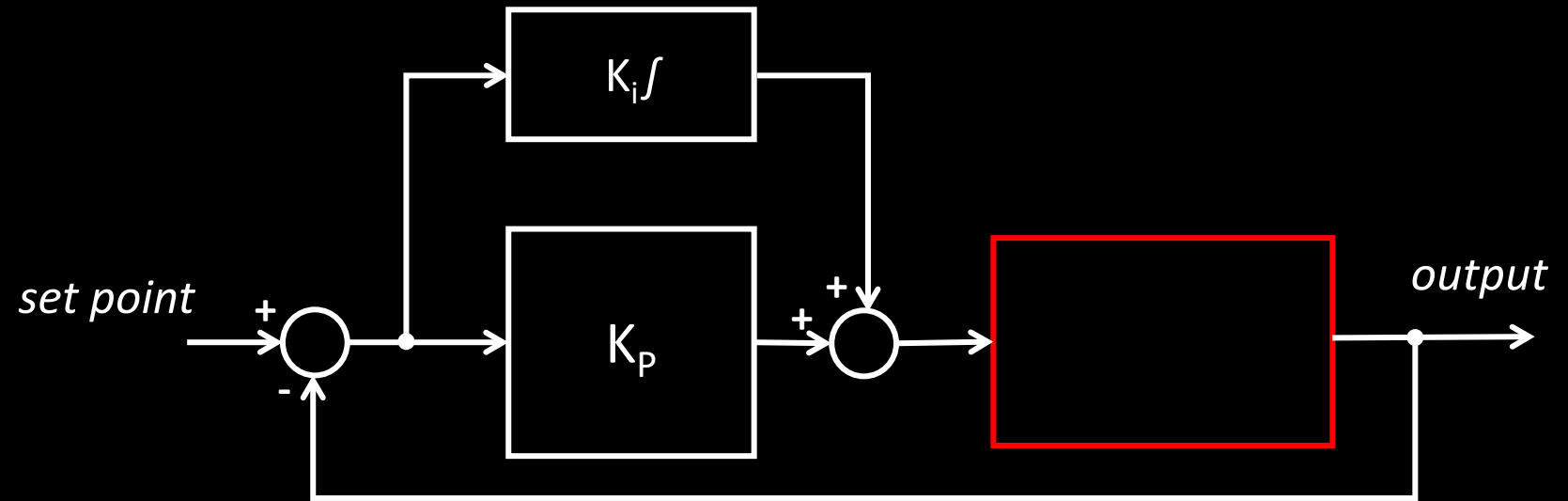


Integrator output

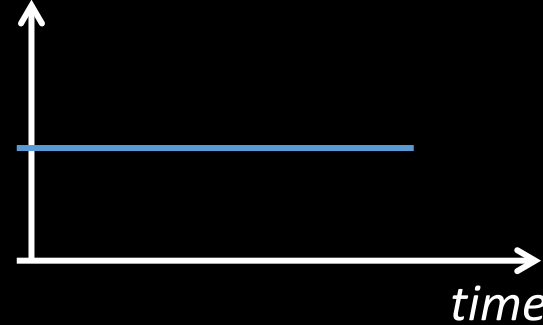


PID control

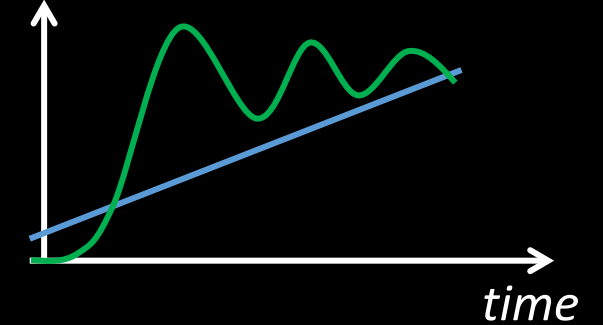
- Drone example



steady state error

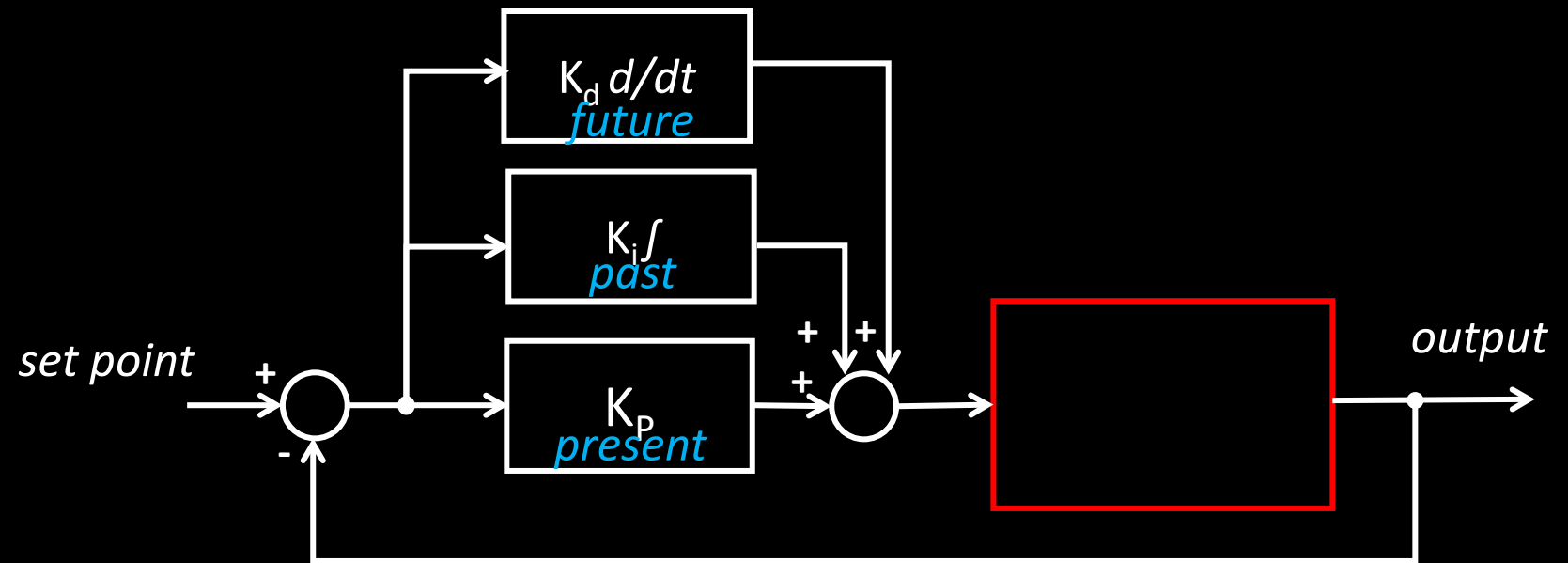


Integrator output

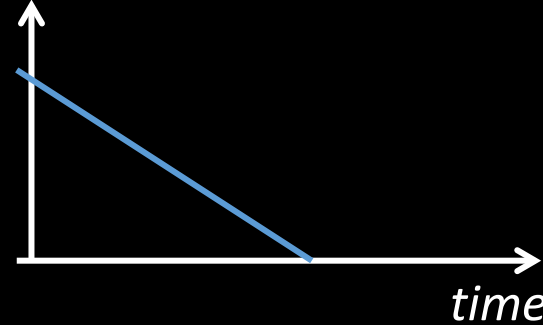


PID control

- Drone example



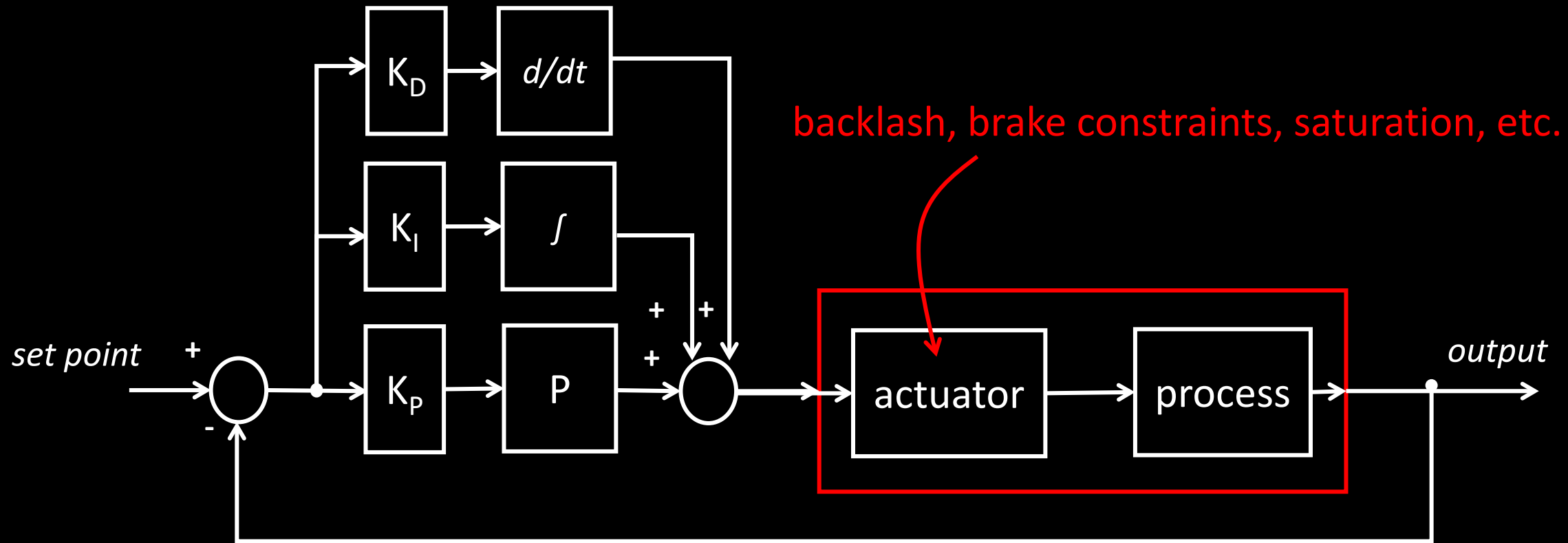
steady state error



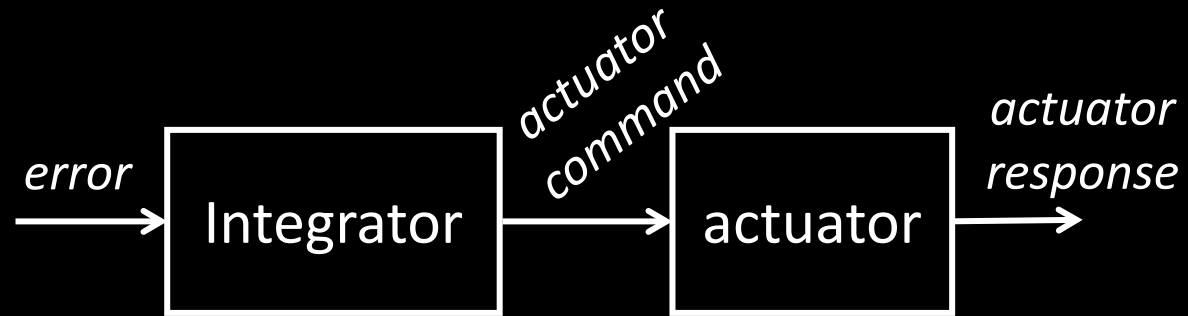
Derivative output



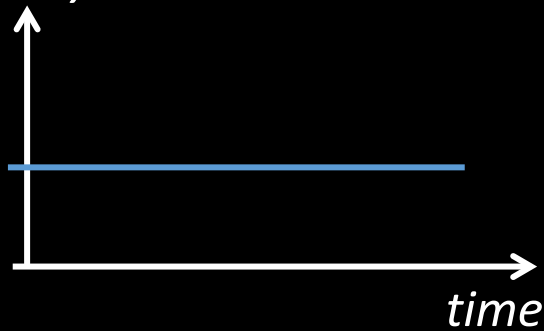
Real Systems are not linear!



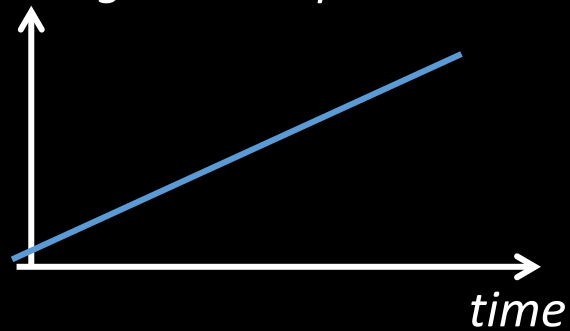
Real Systems are not linear!



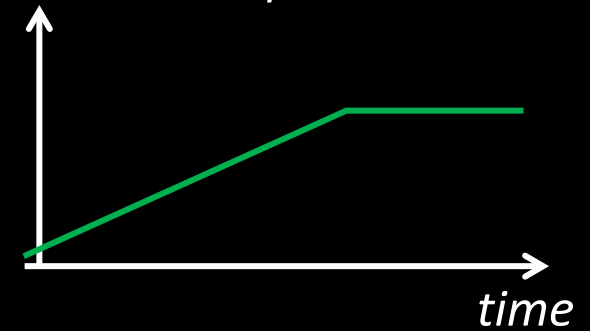
steady state error



Integrator output

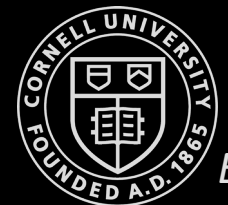
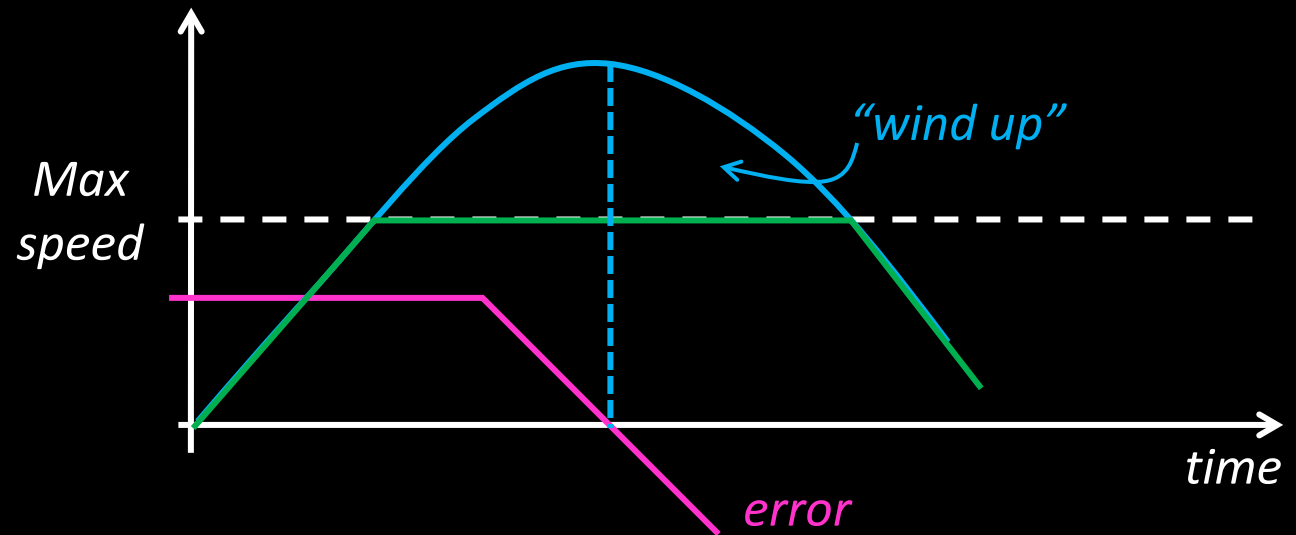
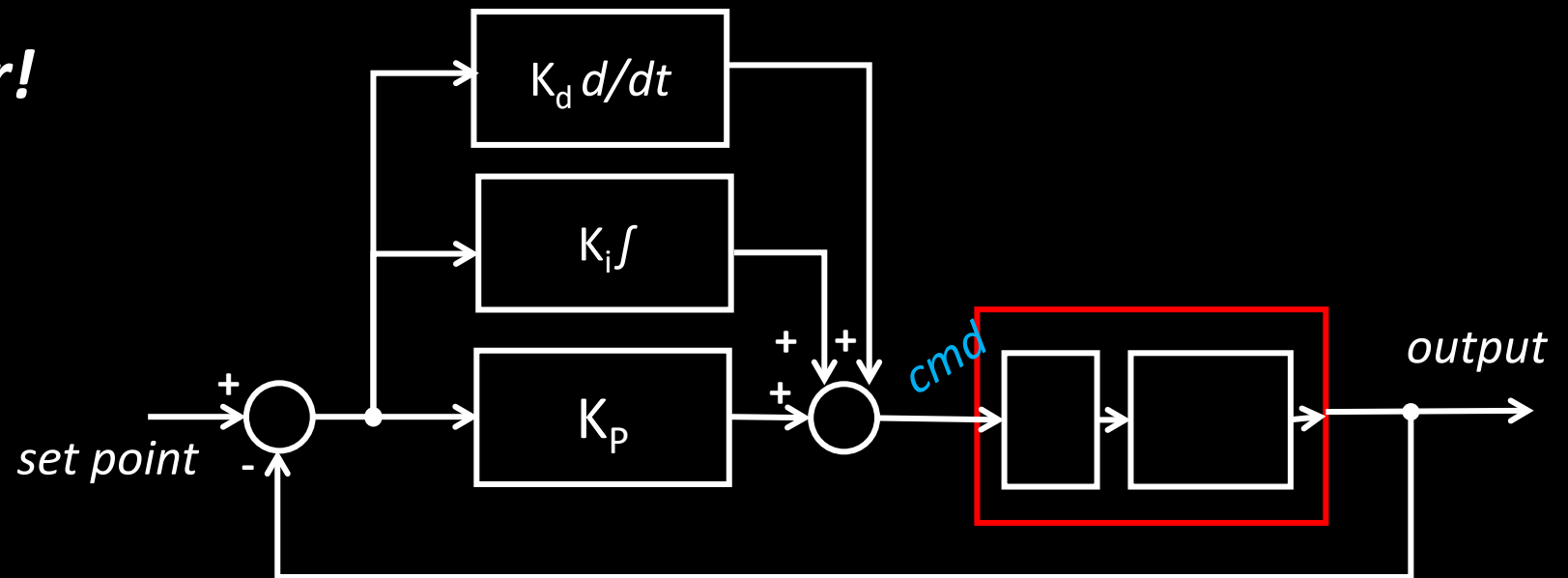


Actuator output



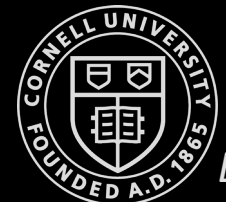
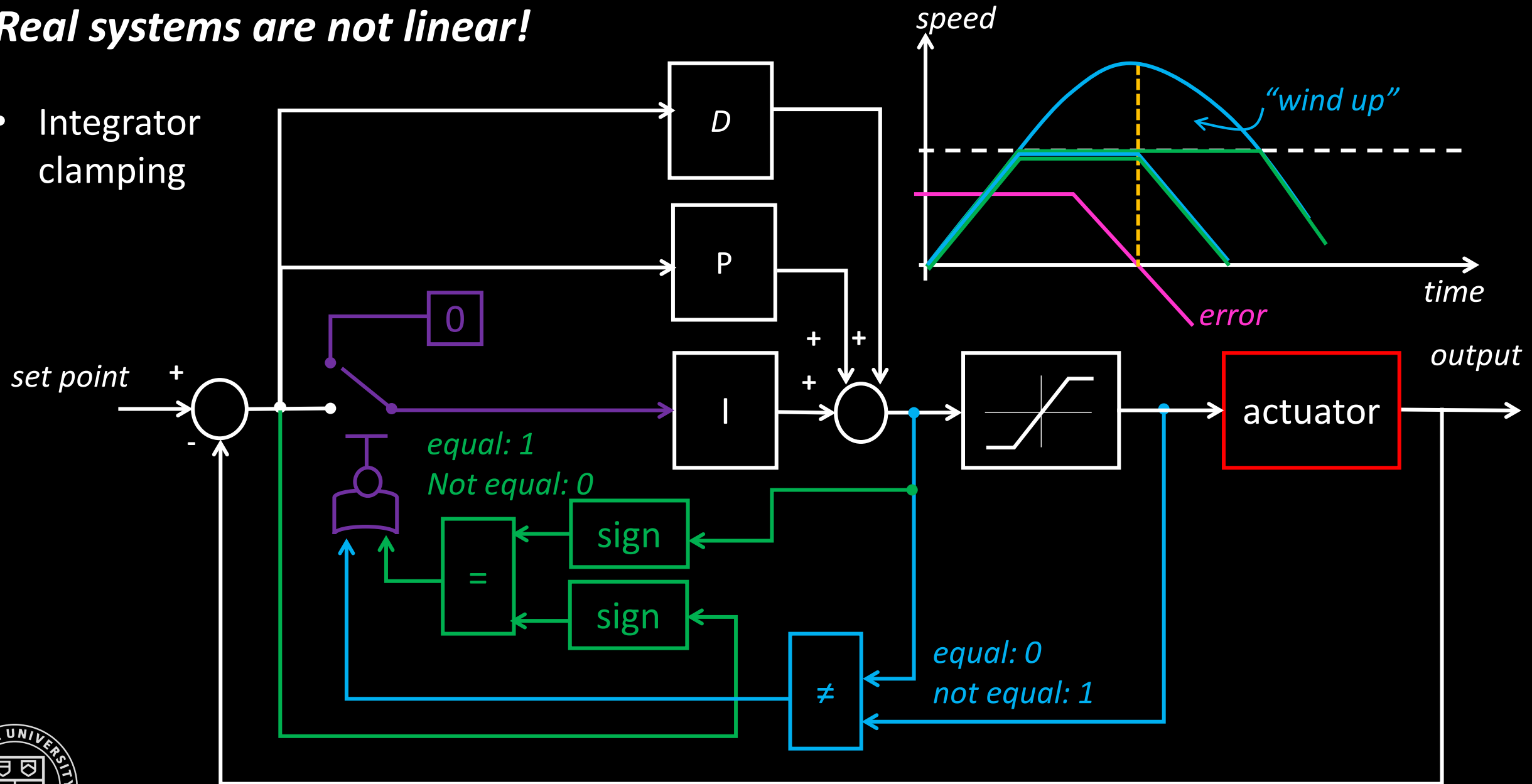
Real systems are not linear!

- Drone example
 - “Integral wind-up”
 - Clamping



Real systems are not linear!

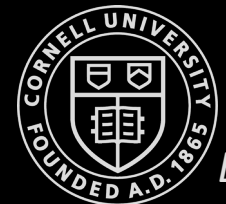
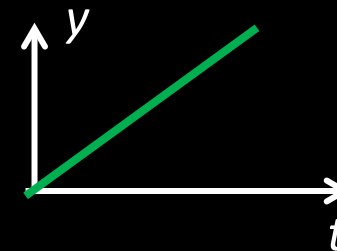
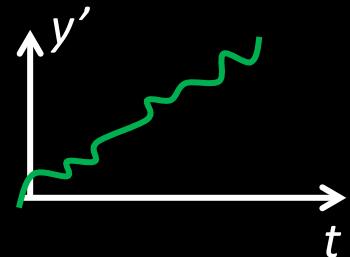
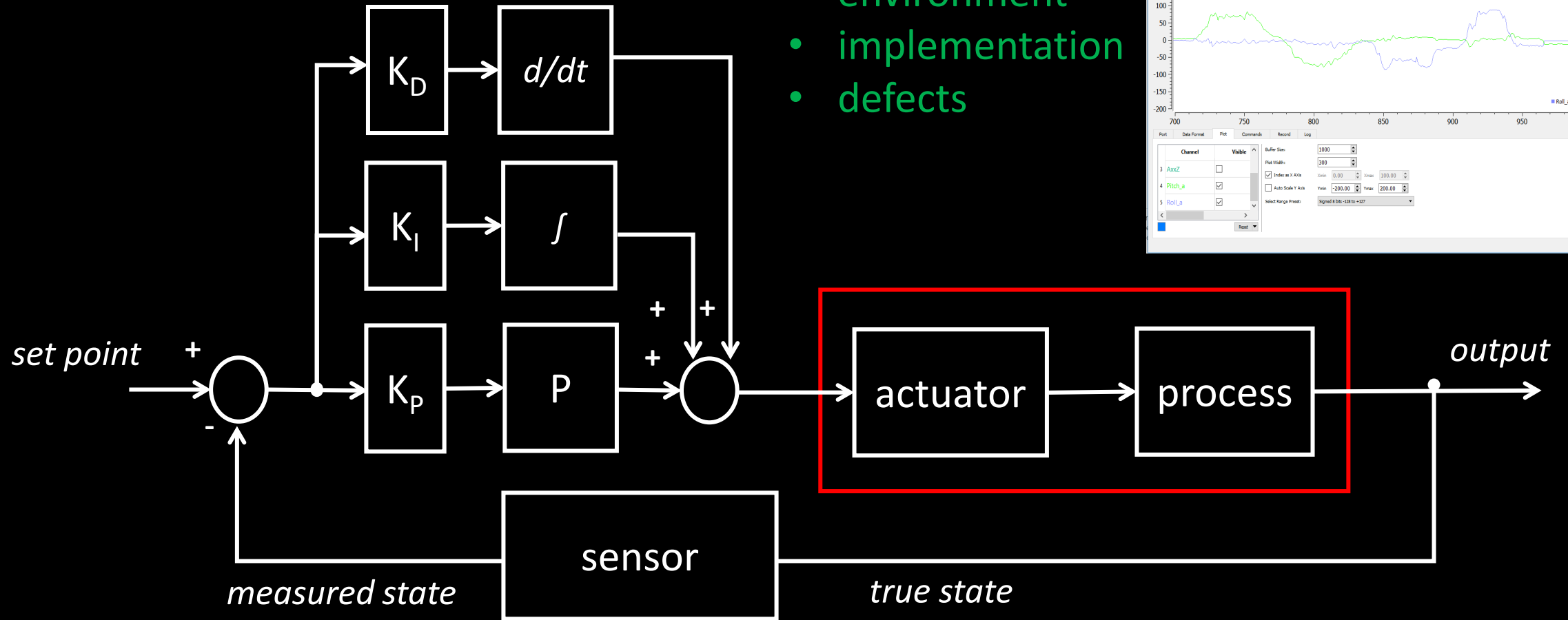
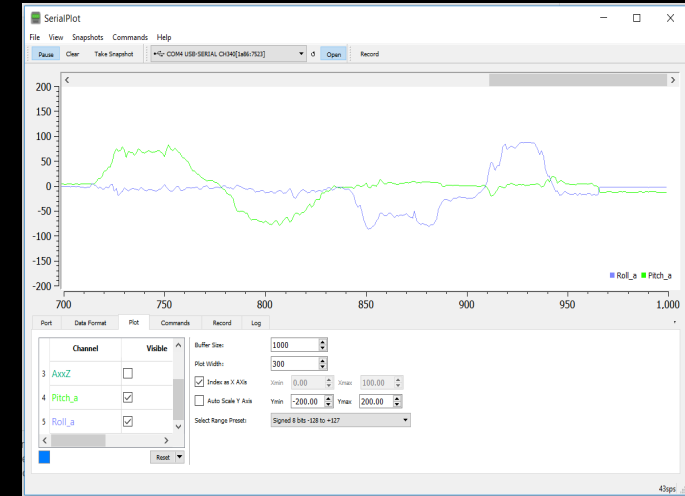
- Integrator clamping



PID and Sensor noise

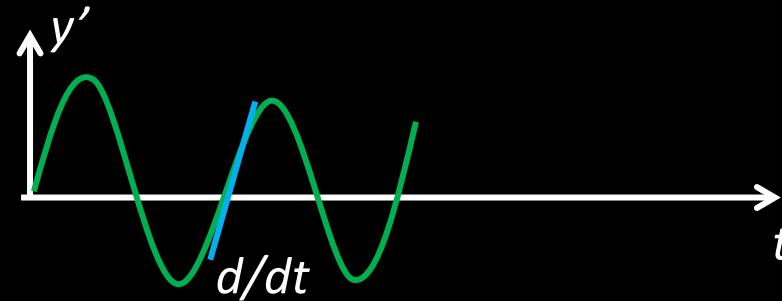
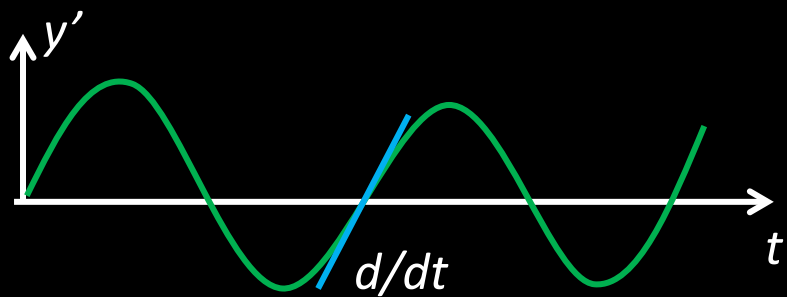
“noise”:

- environment
- implementation
- defects



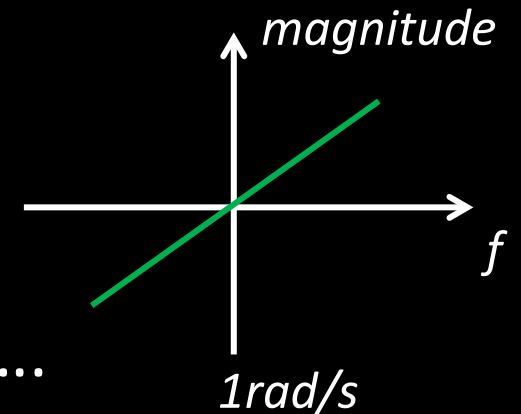
PID and Sensor noise

- Derivatives amplify HF signals more than LF signals

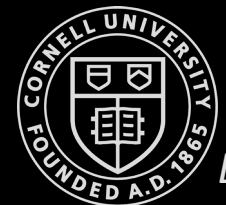


$$y(t) = A\sin(\omega_a t + \phi_a) + B\sin(\omega_b t + \phi_b) + \dots$$

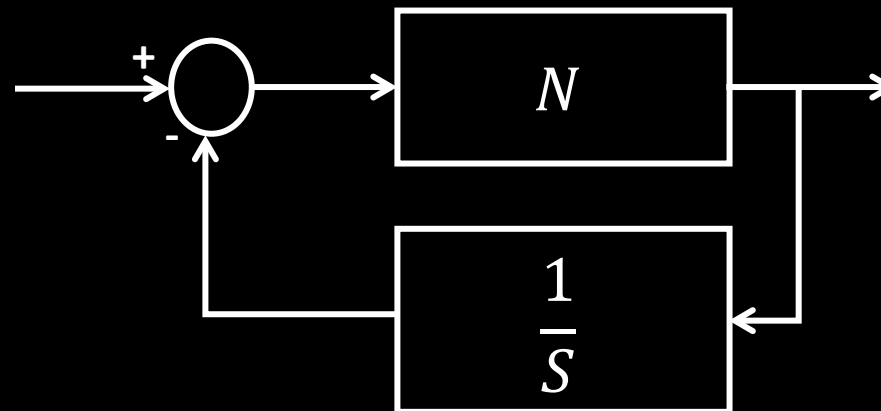
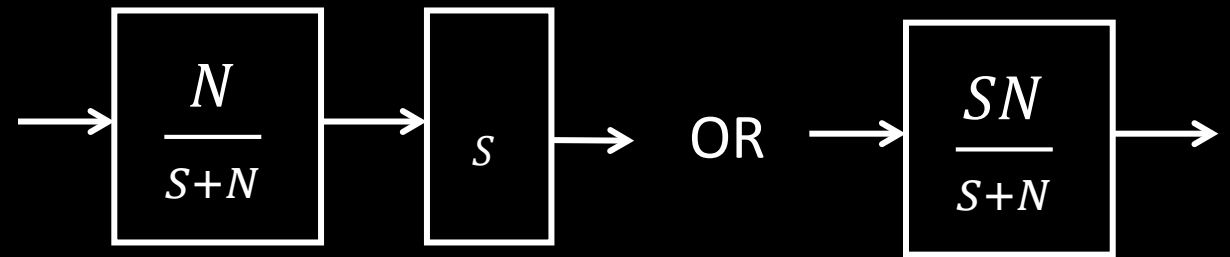
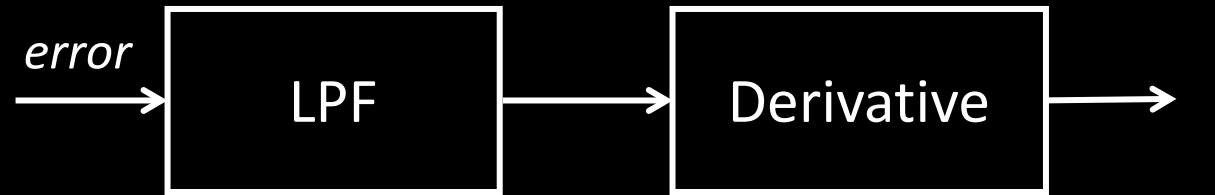
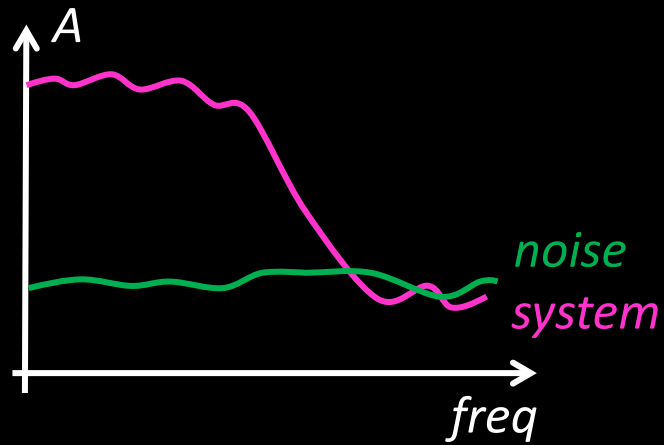
$$dy(t)/dt = A\omega_a \sin(\omega_a t + \phi_a + 90^\circ) + B\omega_b \sin(\omega_b t + \phi_b + 90^\circ) + \dots$$



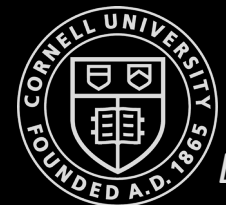
- if $\omega_a > 1\text{rad/s}$, the amplitude will increase
- if $\omega_a < 1\text{rad/s}$, the amplitude will decrease



PID and Sensor noise



Time	Laplace
$\frac{d}{dt}$	S
$\int dt$	$\frac{1}{S}$
1 st order LPF	$\frac{N}{S+N} = \frac{1}{\frac{1}{N}S+1} = \frac{1}{\tau S+1}$



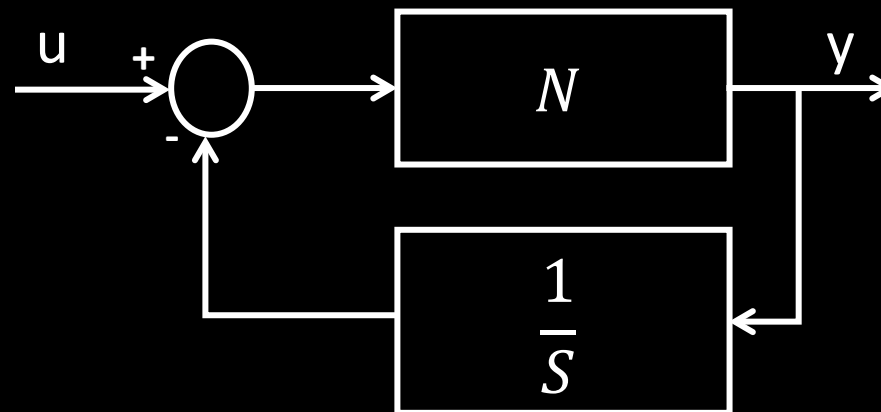
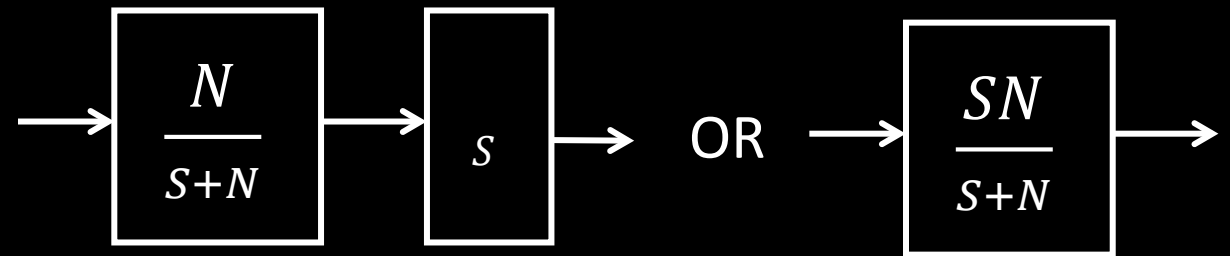
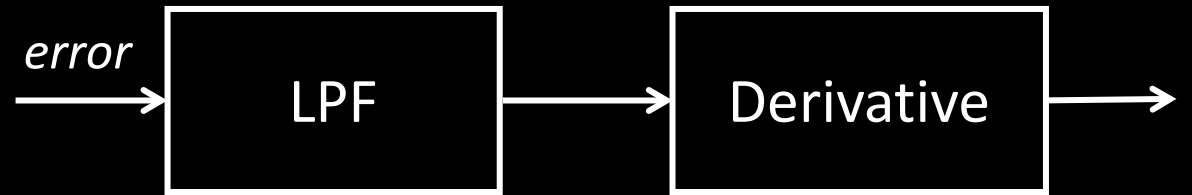
PID and Sensor noise

$$y = N \left(u - \frac{y}{s} \right)$$

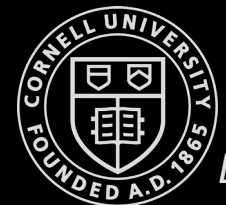
$$y + \frac{Ny}{s} = Nu$$

$$y = \frac{N}{1 + \frac{N}{s}} u$$

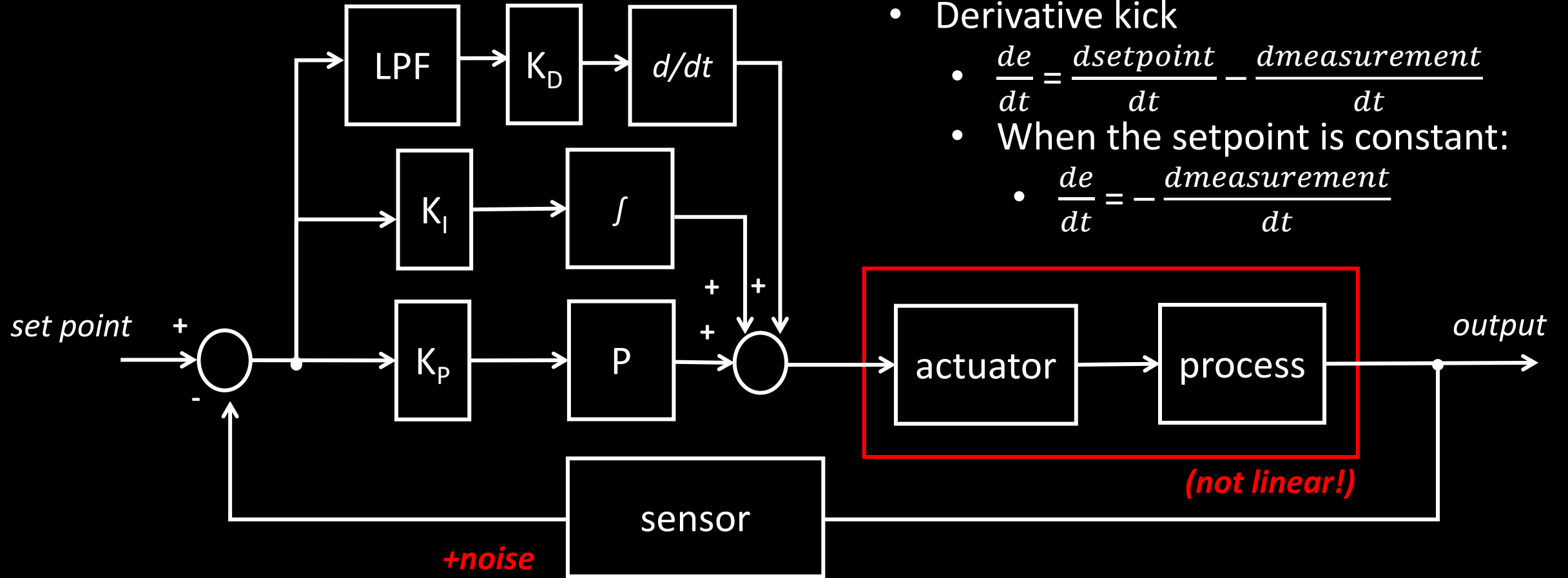
$$\frac{y}{u} = \frac{N}{1 + N\frac{1}{s}}$$



Time	Laplace
$\frac{d}{dt}$	S
$\int dt$	$\frac{1}{S}$
1 st order LPF	$\frac{N}{S+N} = \frac{1}{\frac{1}{N}S+1} = \frac{1}{\tau S+1}$



PID

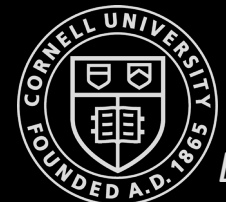


- Integrator wind-up
- Derivative low pass filter
- Derivative kick

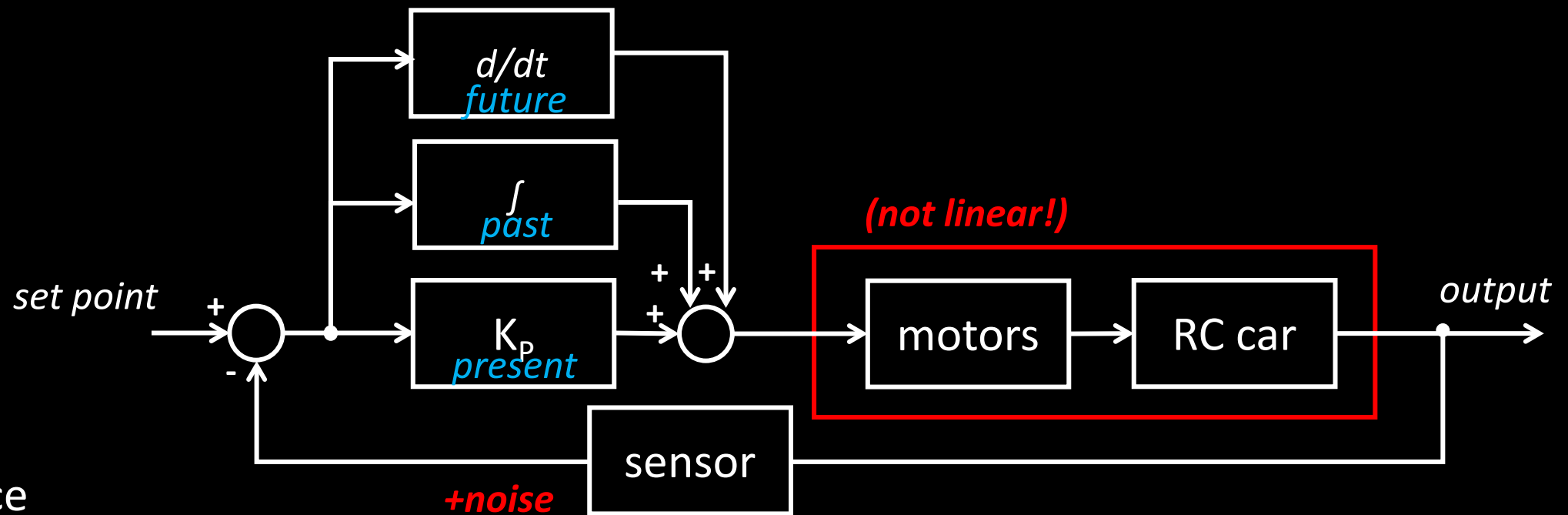
- $\frac{de}{dt} = \frac{d\text{setpoint}}{dt} - \frac{d\text{measurement}}{dt}$

- When the setpoint is constant:

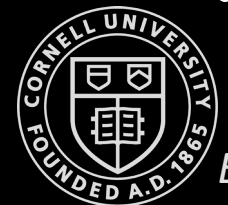
- $\frac{de}{dt} = - \frac{d\text{measurement}}{dt}$



PID control

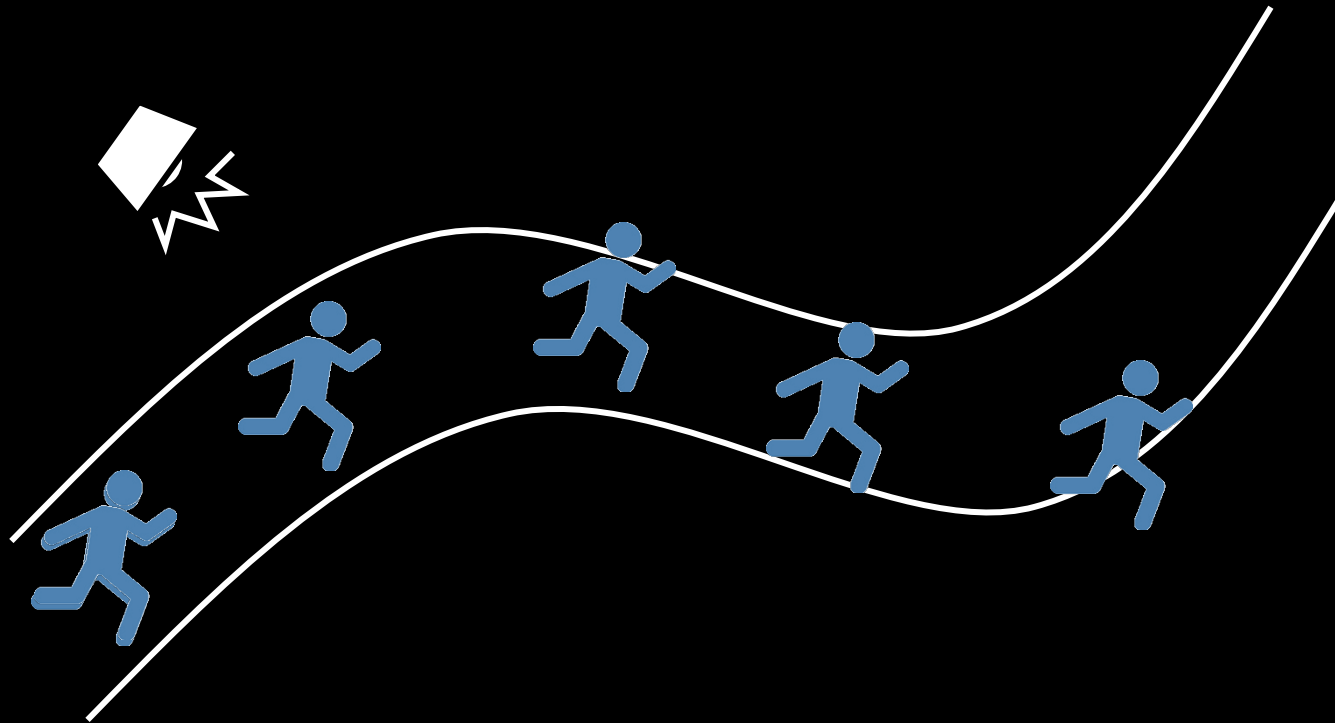


- Performance
 - Rise time/Response
 - Ex: 10% to 90% of final value
 - Peak time
 - Time to reach first peak
 - Overshoot
 - Amount in excess of final value
 - Settling time
 - Ex: Time before output settles to 1% of final value

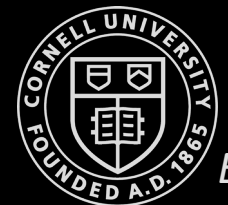
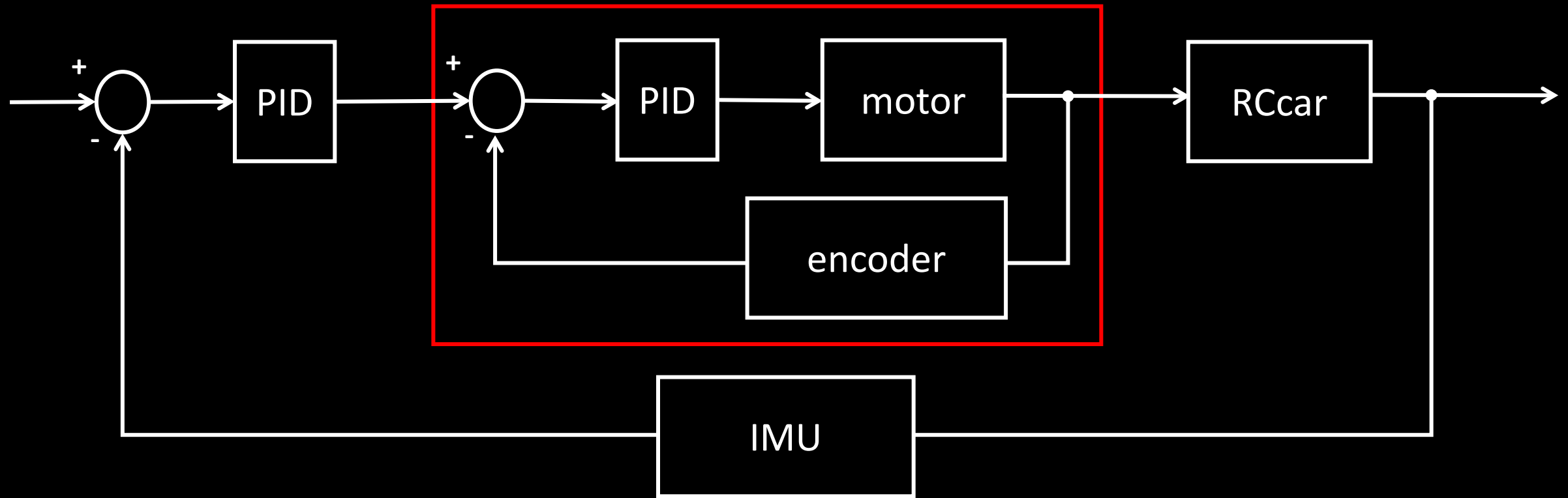


Discrete PID Control

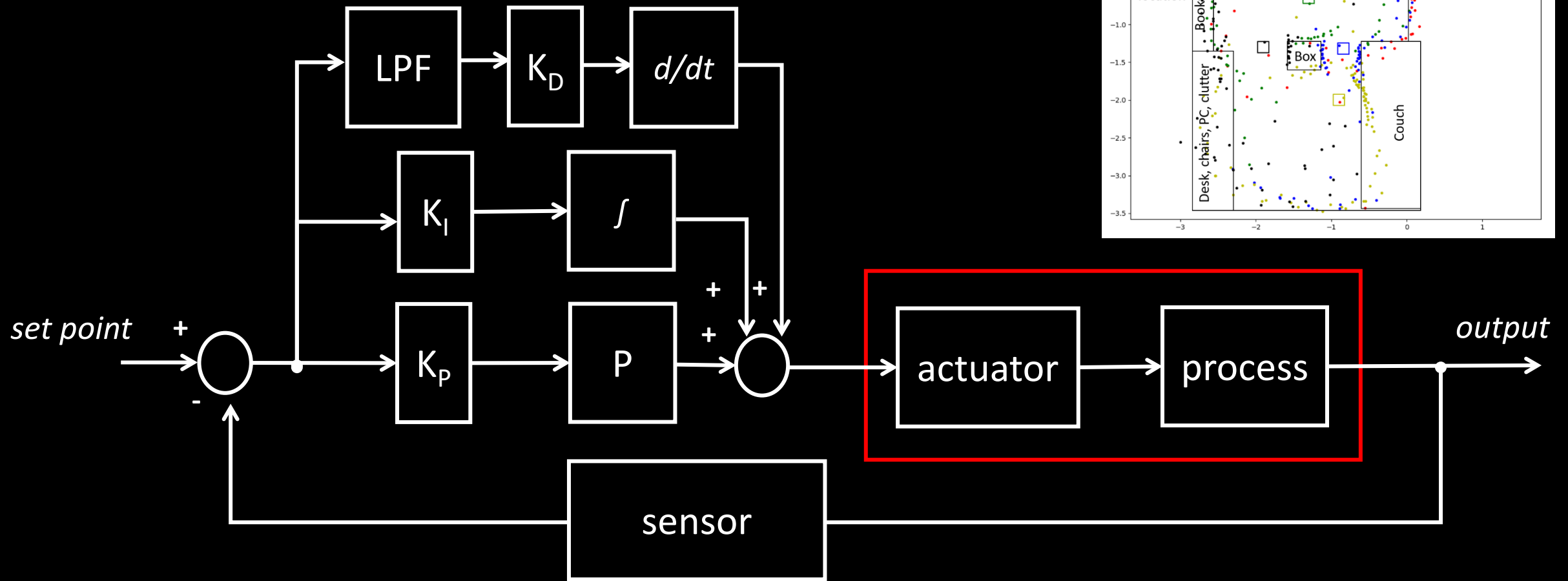
- Sampling time
- Control ~ 10 times faster than the system



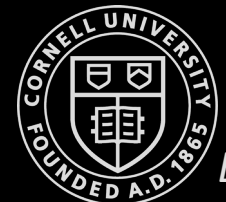
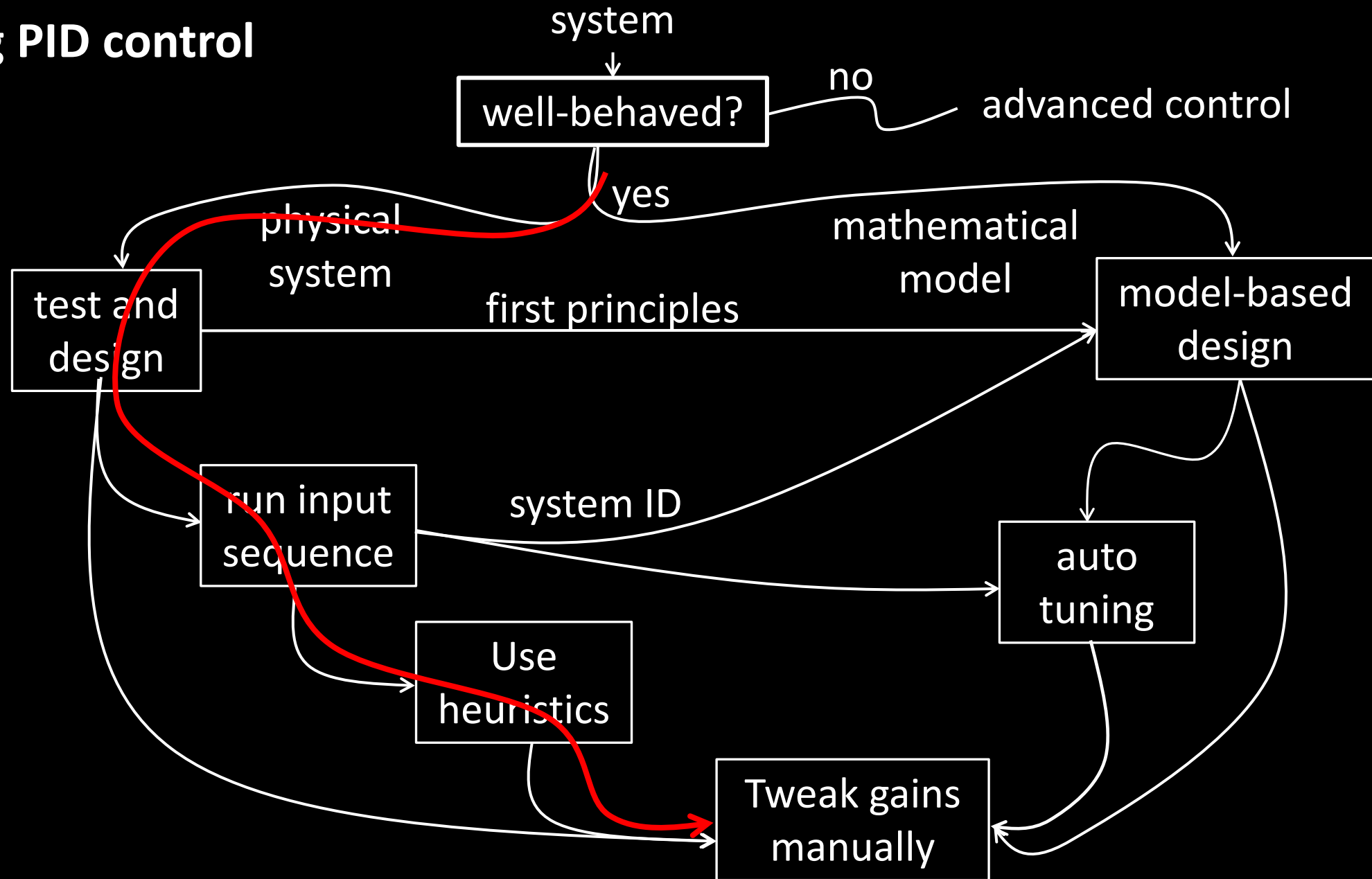
Cascaded Control Loops



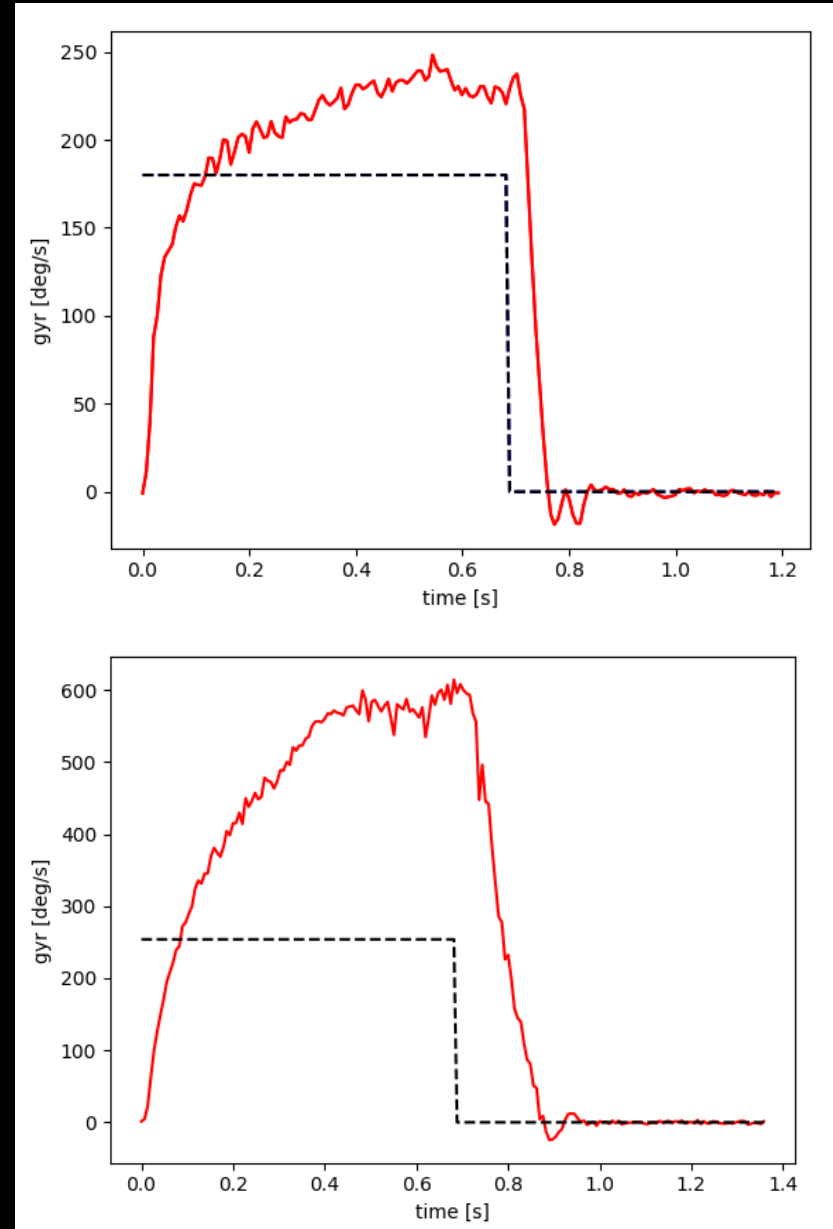
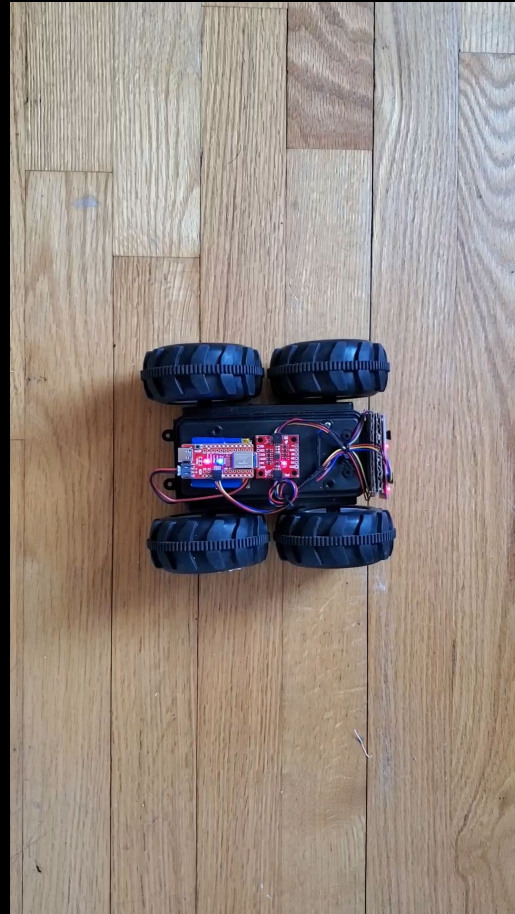
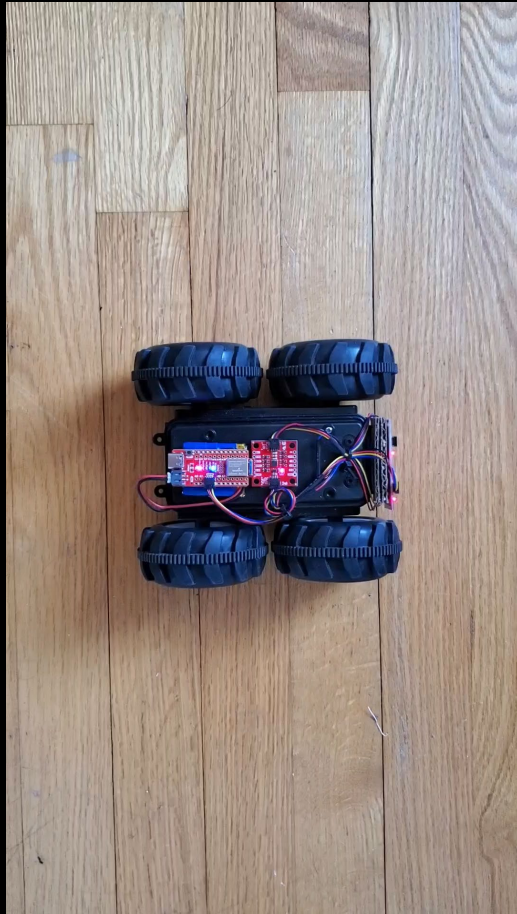
PID



Tuning PID control



Tuning PID control



Tuning PID control

- Chien, Hornes, and Reswick method

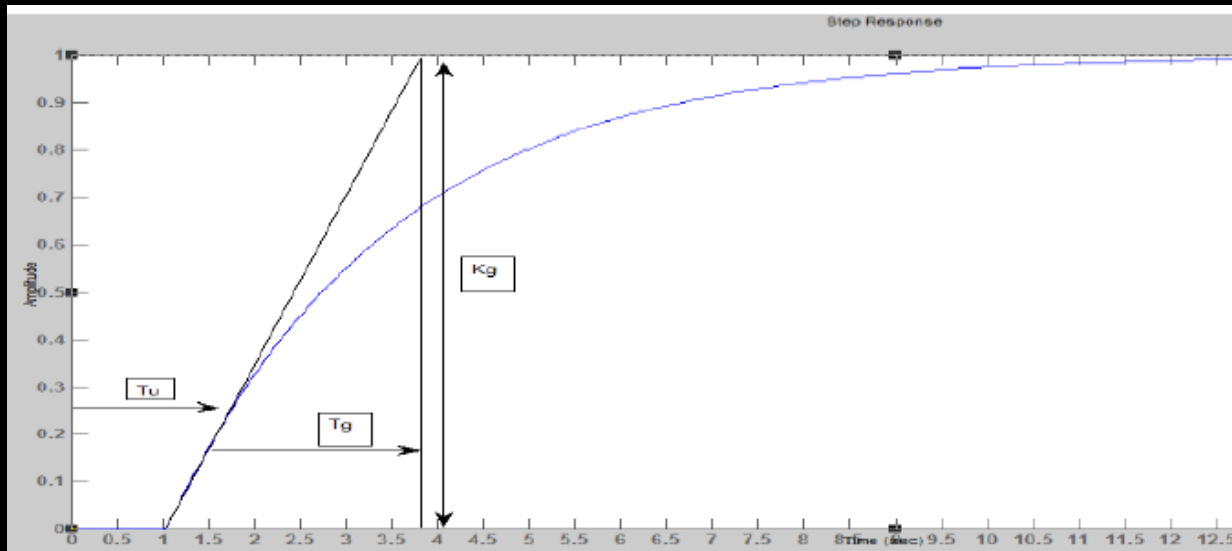
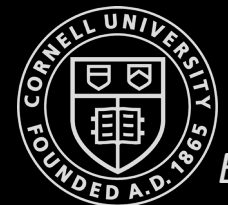
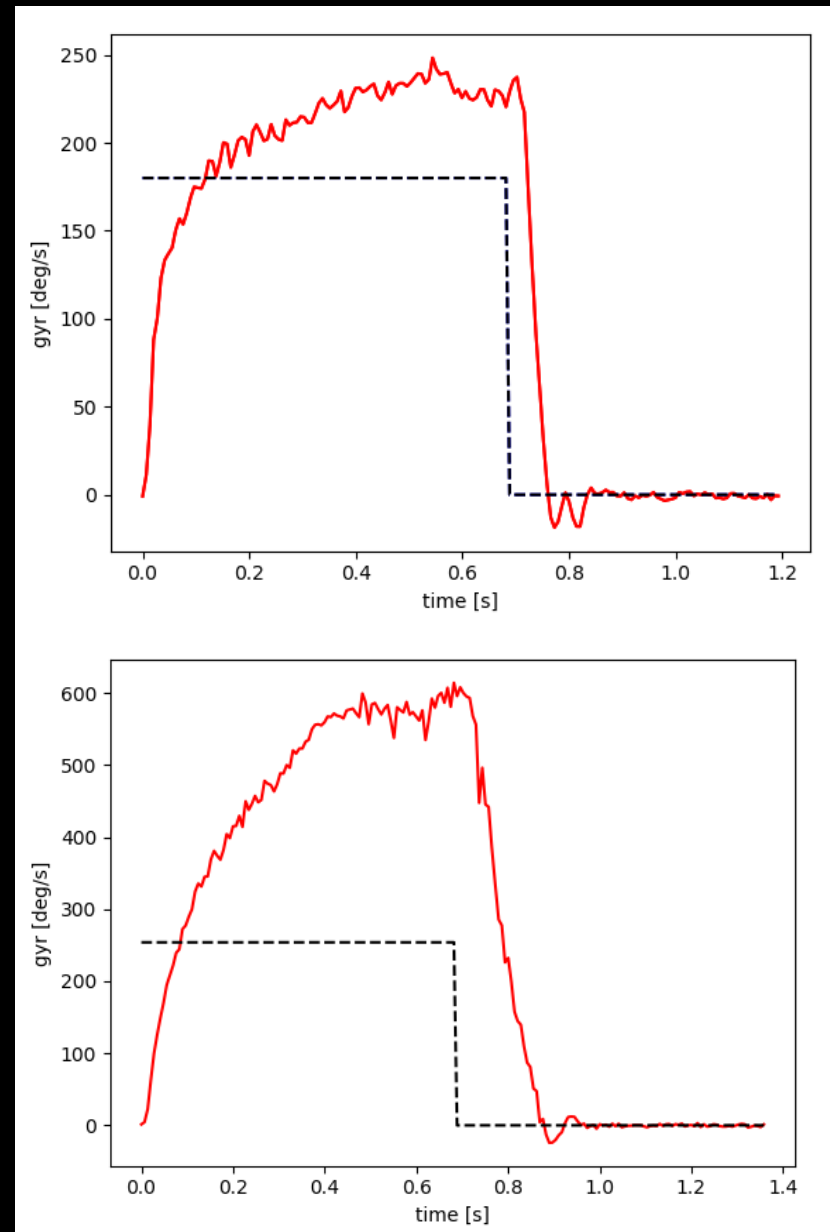


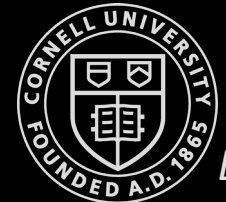
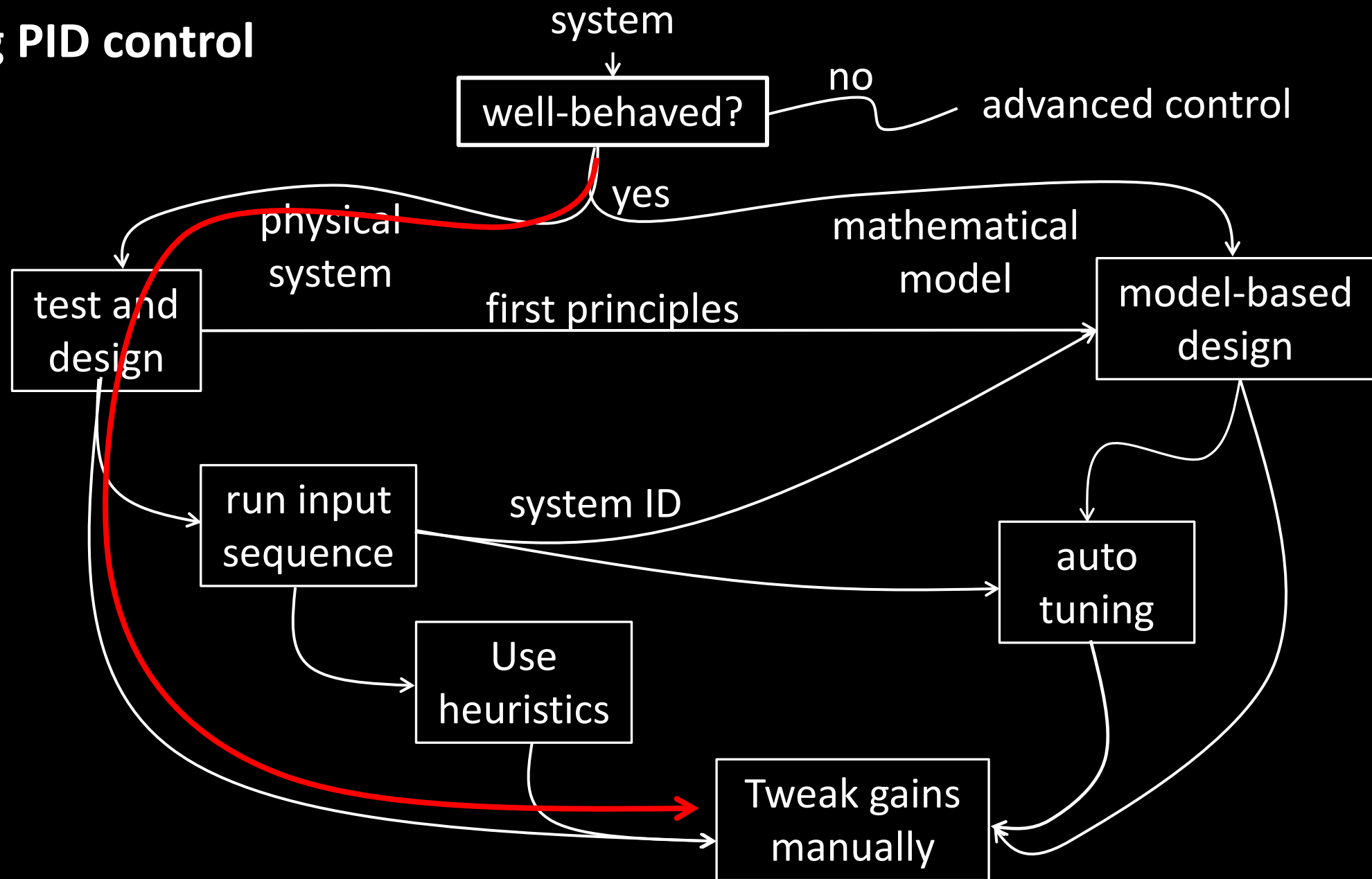
Fig.7. Open loop response of CHR method

Table.11. CHR Compensator

Type of controller	K_p	T_i	T_d
PID	$0.6T_g/T_uK_g$	T_g	$0.5T_u$

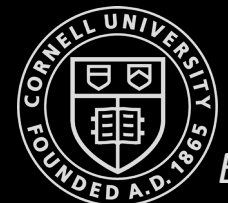


Tuning PID control

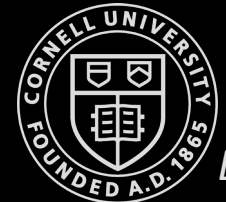
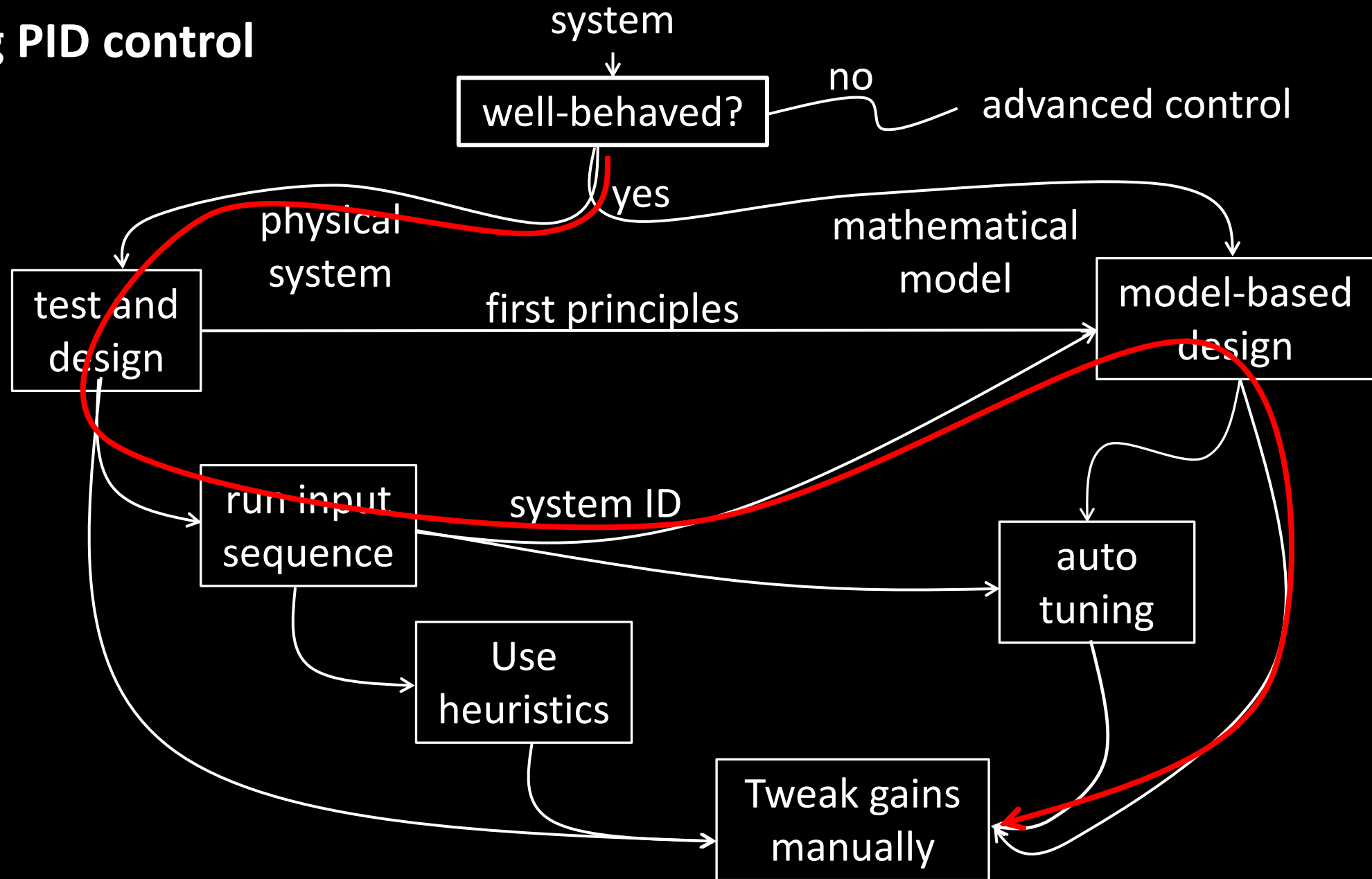


PID control

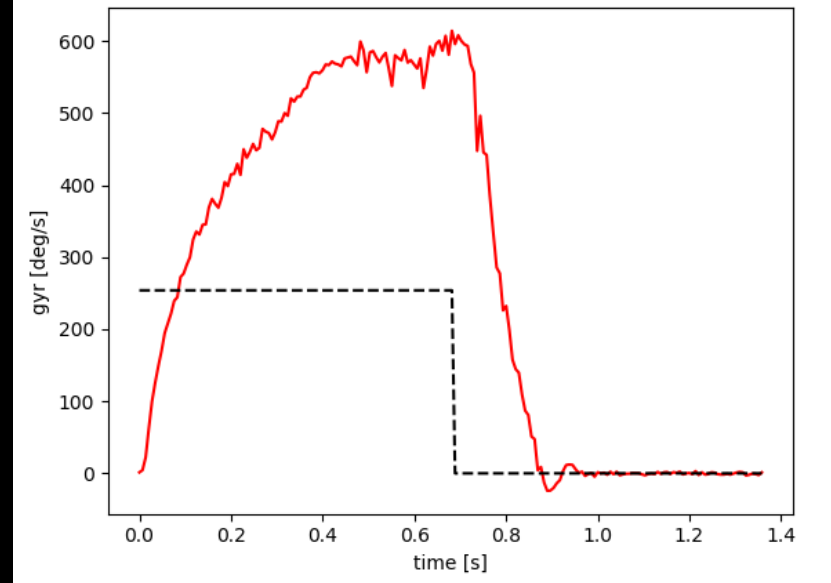
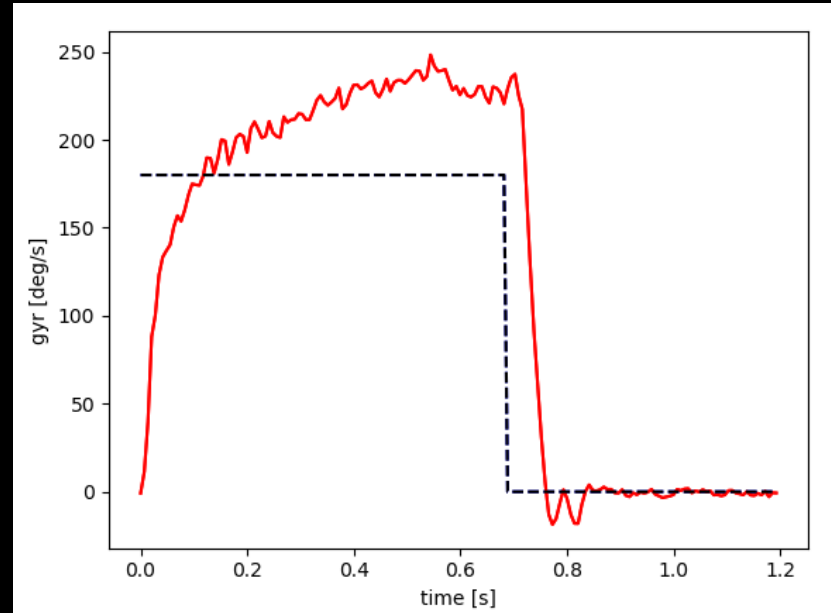
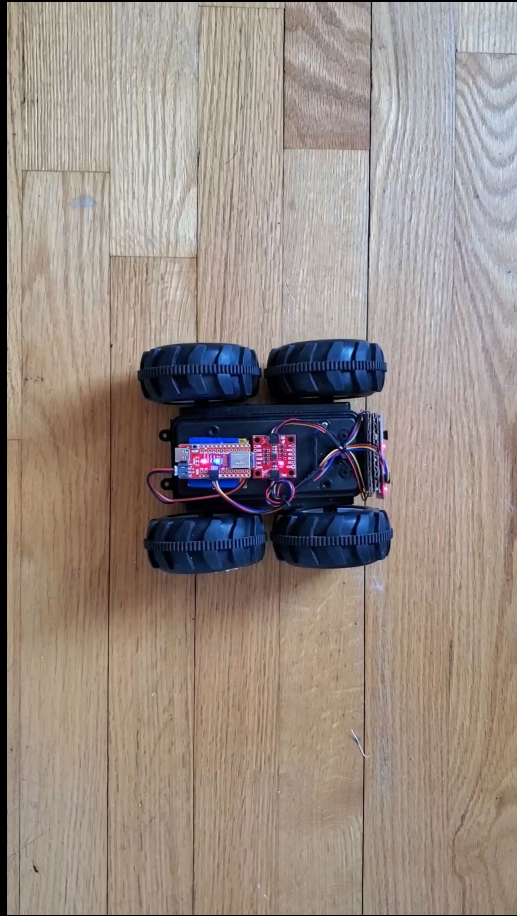
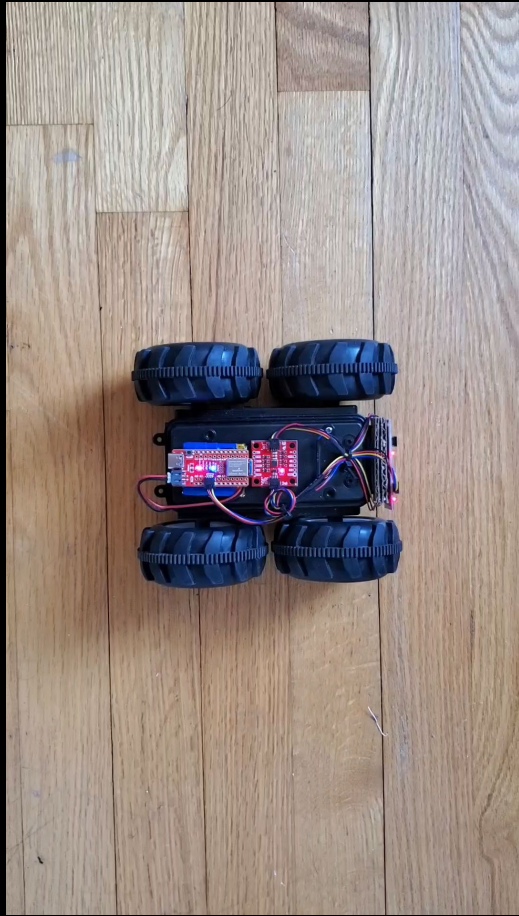
- **Heuristic procedure #1:**
 - Set K_p to small value, K_D and K_I to 0
 - Increase K_D until oscillation, then decrease by factor of 2-4
 - Increase K_P until oscillation or overshoot, decrease by factor of 2-4
 - Increase K_I until oscillation or overshoot
 - Iterate
- **Heuristic procedure #2:**
 - Set K_D and K_I to 0
 - Increase K_P until oscillation, then decrease by factor of 2-4
 - Increase K_I until loss of stability, then back off
 - Increase K_D to increase performance in response to disturbance
 - Iterate



Tuning PID control



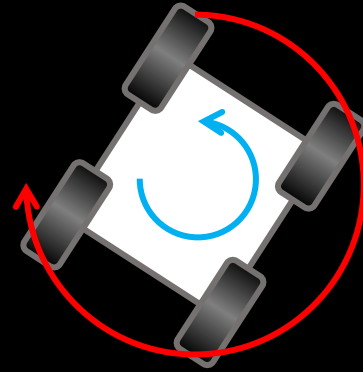
Tuning PID control



Tuning PID control

- Equations of motion

- $x = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$



- <https://tinyurl.com/y67glgzk>

$$F = ma$$

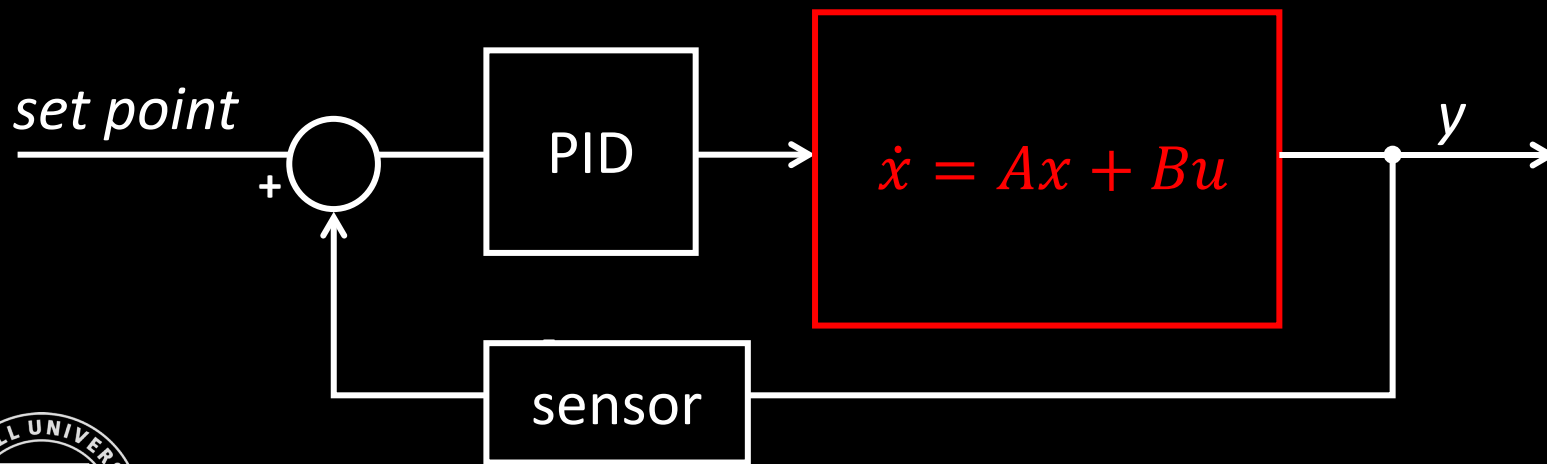
$$\tau = I\alpha$$

$$\tau = I\ddot{\theta}$$

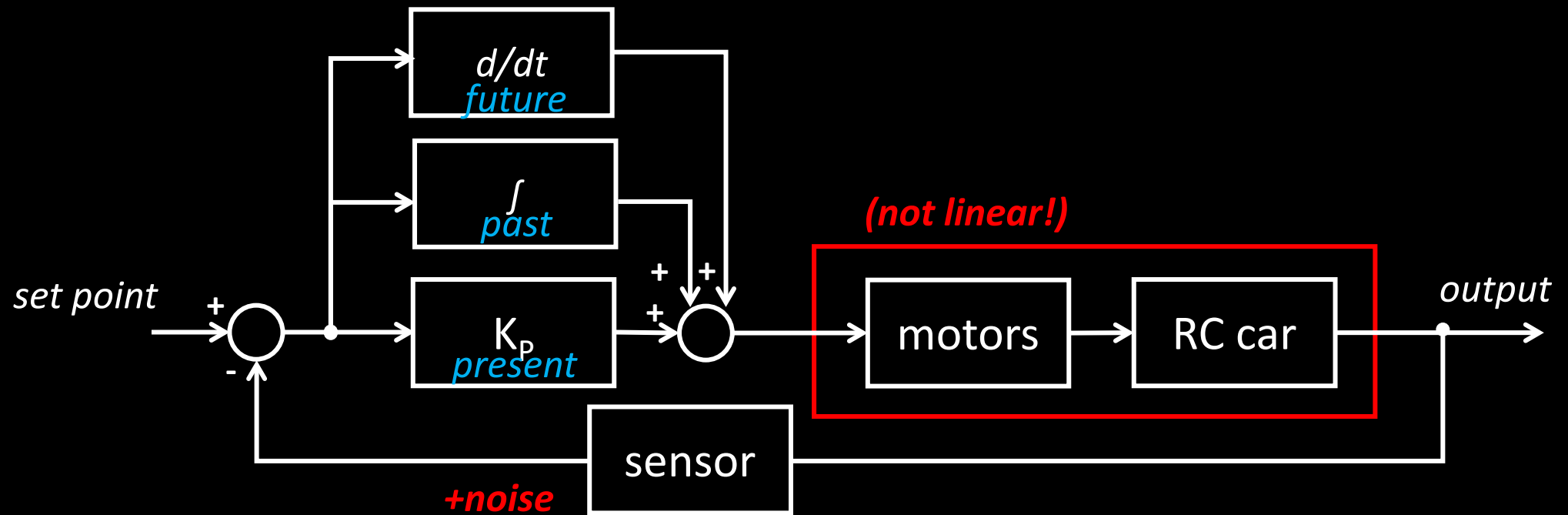
$$u - \dot{\theta}c = I\ddot{\theta}$$

$$\ddot{\theta} = \frac{-\dot{\theta}c}{I} + \frac{1}{I}u$$

$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & \frac{-c}{I} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{I} \end{bmatrix} u$$



PID control



$$\text{1st order system: } \begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & \frac{-c}{I} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{I} \end{bmatrix} u$$

$$\text{2nd order system: } \begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ cst & \frac{-c}{I} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{I} \end{bmatrix} u$$

